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September 1992

# Seamless circular high-temperature austenitic steel tubes

Technical delivery conditions

<u>DIN</u> 17459

Nahtlose kreisförmige Rohre aus hochwarmfesten austenitischen Stählen; technische Lieferbedingungen

In keeping with current practice in standards published by the International Organization for Standardization (ISO), a comma has been used throughout as the decimal marker.

See Explanatory notes for connection with International Standard ISO 2604-2: 1975; published by the International Organization for Standardization.

The symbol ● denotes items which shall, the symbol ●● denoting items which may, be agreed upon at the time of ordering.

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### 1 Scope and field of application

This standard specifies technical delivery conditions for seamless circular tubes made from high-temperature austenitic steel as specified in table 1. Such tubes are intended primarily to be used in high-pressure applications where elevated temperatures and high mechanical stresses are involved (e.g. in the construction of pressure boilers, pressure vessels, pipelines, and in the chemical industry).

### 2 Concepts

2.1 High-temperature austenitic steel is austenitic steel which has a minimum chromium content of 13% by mass and which, when exposed to long-term mechanical stress and temperatures over 550°C, remains strong.

2.2 See DIN 17 014 Part 1 for heat treatment terminology.

### 3 Steel grades

- **3.1** This standard deals with tubes made from the steel grades specified in table 1.
- 3.2 ◆ The steel grade is to be selected by the purchaser.

### 4 Designation and ordering

### 4.1 Standard designation

The standard designation shall give, in the following order:

- a) name of product (tube);
- b) number of the relevant dimensional standard (DIN 2462 Part 1):

Continued on pages 2 and 18

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- c) characteristic dimensions (outside diameter  $\times$  wall thickness, s);
- d) DIN number (DIN 17459);
- e) material designation or number (cf. table 1);
- f) symbol indicating heat treatment condition (cf. table 5).

Designation of a seamless circular tube in compliance with this standard and with DIN 2462 Part 1, with an outside diameter of 38 mm and a wall thickness of 2,6 mm, made of X 6 CrNi t811 steel (material number 1.4948), supplied in the cold formed, heat treated and pickled condition (h or III b):

Tube DIN 2462 - 38  $\times$  2,6 - DIN 17 459 - X 6 CrNi 18 11 h

Tube DIN 2462  $-38 \times 2.6 - DIN 17459 - X 6 CrNi 1811 III b$ 

Tube DIN 2462 - 38  $\times$  2,6 - DIN 17459 - 1.4948 h

Tube DIN 2462 - 38  $\times$  2,6 - DIN 17459 - 1.4948 III b

#### 4.2 • Essential order details

The following order details are essential.

- 4.2.1 Quantity (e.g. total length, number of items or mass).
- 4.2.2 Name of product (tube).
- 4.2.3 Number of relevant dimensional standard (DIN 2462 Part 1)
- 4.2.4 Characteristic dimensions (outside diameter x wall thickness) (cf. DIN 2462 Part 1).
- 4.2.5 DIN number (DIN 17459).
- 4.2.6 Material designation or number (cf. table 1).
- 4.2.7 Symbol denoting heat treatment condition (cf. table 5).
- 4.2.8 Type of length (cf. DIN 2462 Part 1).
- 4.2.9 Tolerance class for outside diameter and wall thickness (cf. DIN 2462 Part 1).
- 4.2.10 Type of DIN 50 049 inspection document (cf. subclause 6.1) and, in the case of third party inspection, the testing agency and any specifications to be complied with. Example of an order:

100 m of seamless circular tube complying with DIN 2462 Part 1 and with this standard, with an outside diameter of 38 mm and a wall thickness of 2,6 mm, made of X 6 CrNi 18 11 steel (material number 1.4948), condition on supply h, in specified lengths of 6 m, belonging to tolerance class D2, T3, to be supplied with a DIN 50 049 - 3.1.B inspection document, shall be ordered as:

100 m tube DIN 2462  $-38 \times 2,6$ 

DIN 17459 - X 6 CrNi 1811 - h In specified lengths of 6 m, tolerance class D2, T3, with DIN 50049 - 3.1.B inspection document

#### 4.3 •• Optional order details

The essential order details may, if so agreed, be supplemented by one or more of the following items and tests.

- 4.3.1 The steelmaking process used (cf. subclause 5.1.1).
- 4.3.2 The manufacturing process used (cf. subclause 5.1.2.1).

- 4.3.3 Non-destructive testing for determining longitudinal and transverse imperfections (cf. subclause 5.10.2).
- 4.3.4 Ultrasonic testing of tubes made from 1.4959 steel (cf. subclause 5.10.3).
- 4.3.5 Non-destructive testing of tubes with an outside diameter not exceeding 20 mm and a wall thickness not exceeding 2 mm (cf. subclause 5.10.4).
- 4.3.6 Sizes of tubes if other than specified here (cf. subclause 5.11.2).
- 4.3.7 Cross section of tubes if other than circular (cf. subclause 5.11.3).
- 4.3.8 Determination of elevated temperature 0,2 % or 1 % proof stress (cf. subclause 6.3.1.4).
- 4.3.9 Chemical composition as determined by product analysis (cf. subclause 5.3.2).
- 4.3.10 Internal hydrostatic pressure testing at a higher pressure than specified here (cf. subclause 6.5.9).
- 4.3.11 Method of tightness testing to be used (cf. subclause 6.5.9).
- 4.3.12 Continuous marking (cf. subclause 7.3).

Example of an order with optional details:

100 m of seamless circular tube complying with DIN 2462 Part 1 and this standard, with an outside diameter of 38 mm and a wall thickness of 2,6 mm, made from X 6 CrNi 18 11 steel (material number 1.4948), as delivered condition m, in specified lengths of 6 m, belonging to tolerance class D2, T3, where the tube has been tested non-destructively, with verification of elevated temperature proof stress, to be supplied with a DIN 50 049 - 3.1.C inspection document, shall be ordered as:

100 m tube DIN 2462 - 38 x 2,6 DIN 17459 - X 6 CrNi 1811 - m in specified lengths of 6 m, tolerance class D2, T3, with DIN 50049 - 3.1.C inspection document, tested non-destructively -300 °C proof stress

### 5 Requirements

### 5.1 Manufacturing process

- 5.1.1 Unless otherwise specified, the steelmaking process shall be at the manufacturer's discretion.
- •• If so agreed, the purchaser shall be informed of the steelmaking process used.
- 5.1.2 Tubes are normally produced by hot or cold rolling, hot pressing or cold drawing, or a combination of these processes. The manufacturing process shall be at the manufacturer's discretion.
- 5.1.2.1 •• If so agreed, the purchaser shall be informed of the manufacturing process used.

#### 5.2 As delivered condition

Tubes shall be supplied in one of the conditions specified in tables 3 and 5. The solution heat treatment temperature of hot pressed tubes shall be as specified in table A.3, with quenching in water (with the exception of grade X 8 CrNiMoVNb 1613).

#### 5.3 Chemical composition

The chemical composition, as determined by ladie analysis, shall be in compliance with table 1.

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#### 5.3.2 Product analysis

5.3.2.1 •• A product analysis may be agreed at the time of ordering. Where such an analysis is carried out, the results may deviate from the values given in table 1 by the amounts listed in table 2.

#### 5.3.3 Deviations

With the consent of the purchaser, minor deviations of the chemical composition from the limiting values specified are permitted, provided they do not adversely affect the mechanical properties and weldability of the tube.

#### 5.4 Mechanical properties

- **5.4.1** The values of 0,2% and 1% proof stress, tensile strength, elongation at fracture and impact energy at ambient temperature shall comply with the values given in table 3.
- 5.4.2 The elevated temperature 0,2 % and 1 % proof stress shall be as specified in table 4.
- 5.4.3 The values specified in tables 3 and 4 apply for the conditions specified in subclause 5.2, under the conditions of test specified in clause 6.
- 5.4.4 Guideline values for rupture stress are given in appendix A, table A.1.

### 5.5 Technological properties

5.5.1 Tubes shall pass the tests referred to in subclauses 6.5.4 and 6.5.7. Note that tubes as specified here are suitable for both hot and cold forming.

#### 5.6 Weldability

- 5.6.1 Tubes as covered here are suitable for arc welding.
- 5.6.2 The steels specified here may not be suitable for all welding operations, as the behaviour of steel during and after welding changes as a function of the material, form and size of the component, and of the manufacturing and service conditions (cf. DIN 8528 Part 1).
- 5.6.3 Any filler metal required shall be selected, on the basis of DIN 8556 Part 1, as a function of the intended application, the expected stresses, the welding process and conditions in service, due consideration being given to other relevant technical specifications.

### 5.7 Heat treatment and hot forming

Guideline temperatures for heat treatment and hot forming are given in table A.3.

### 5.8 Heat treatment condition and surface quality

- 5.8.1 Tubes shall be supplied in one of the conditions specified in table 5, this being at the purchaser's discretion.
- 5.8.2 Tubes shall have a smooth inner and outer surface, consistent with the manufacturing process used.
- 5.8.3 Slight irregularities in the surface resulting from the manufacturing process (e.g. excess weld metal, raised spots, pit marks, scores) are permitted, provided the thickness tolerance is not exceeded (cf. subclause 5.11.1) and the performance of the tubes is not adversely affected.
- 5.8.4 Dressing of imperfections (e.g. by grinding) is permitted, provided the thickness after dressing continues to meet the requirements specified in subclause 5.11.1. Repair of surface defects by hammering is not permitted.

### 5.9 Tightness

Tubes shall be subjected to tightness testing under the conditions specified in subclause 6.5.9.

#### 5.10 Imperfections

Cf. subclauses 6.5.11 to 6.5.14,

## 5.11 Dimensions, tolerances and mass per unit length

- 5.11.1 The dimensions, tolerances and mass per unit length of tubes shall be as specified in DIN 2462 Part 1.
- 5.11.2 •• If so agreed, tube sizes other than specified in DIN 2462 Part 1 may be supplied.
- 5.11.3 •• If so agreed, non-circular (e.g. oval) tubes may be supplied.

#### 6 Testing

#### 6.1 Inspection documents

Tubes complying with this standard shall be supplied with one of the following DIN 50 049 (EN 10 204) inspection documents:

- a) EN 10 204 inspection certificate A;
- b) EN 10 204 inspection certificate B;
- c) EN 10 204 inspection certificate C;
- d) EN 10 204 inspection report.
- 6.1.1 The certificate or report shall include the following particulars:
- a) the results of testing as described in subclause 6.5;
- the titles of any technical specifications on which testing for compliance with requirements is based;
- the results of ladle analysis for all elements specified in table 1 for the relevant steel grade (this may also be given in an EN 10 204-2.2 inspection document).
- d) marking (cf. clause 7).
- 6.1.2 Where any of the optional tests listed in subclause 4.3 have been agreed, the test results shall be given in an EN 10 204-3.1.B inspection document.

#### 6.2 Test site

Tubes shall be tested at the manufacturer's works. Where an inspector (of a testing agency) is responsible for testing, production shall not be unduly disturbed. A summary of scope of testing and inspection documents is given in table 6.

#### 6.3 Scope of testing

- 6.3.1 Tubes shall be tested by batches.
- 6.3.1.1 Tubes shall be separated into batches according to material, cast, size (wall thickness) and, if necessary, heat treatment condition, each batch consisting of 100 tubes. Tubes may also be separated according to as manufactured length.

Remainders of up to 50 units may be distributed uniformly among the other batches, remainders of over 50 units and consignments of less than 50 units being considered a whole batch.

- 6.3.1.2 One tube shall be taken as a sample from each batch, from which test pieces are then taken. The following tests shall be carried out on the sample:
- a) one tensile test at ambient temperature; where tubes with an outside diameter of 200 mm or more and a wall thickness of 12 mm or more are used as pressure vessel shells, 10% of the tubes per batch shall be tested;
- b) one set of test pieces shall be taken for impact testing from samples with a wall thickness of 20 mm or more; where tubes are used as pressure vessel shells, 10 % of the tubes per batch shall be tested.

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6.3.1.3 •• If so agreed, one product analysis per cast shall be performed.

6.3.1.4 •• Where determination of the 0,2% and 1% proof stress has been agreed, the test temperature and scope of testing shall also be the subject of agreement.

**6.3.1.5** Where s does not exceed 40 mm, each tube or as manufactured length shall undergo a flattening, expanding ring, or ring tensile test as a function of the outside diameter (cf. table 7). If required by the manufacturer, a drift expanding test may be performed instead of an expanding ring test.

**6.3.1.6** Where s exceeds 40 mm, both ends of the tube over a length of 25 mm shall undergo non-destructive testing as described in subclause 6.5.10.

**6.3.1.7** Only 10 % of the tubes in one batch need undergo ultrasonic testing as described in *Stahl-Eisen-Prüfblatt* (Iron and steel test sheets) 1915 and 1918.

6.3.1.8 Tubes with an outside diameter exceeding 20 mm or a wall thickness exceeding 2 mm (with the exception of grade X 8 NiCrAITi 32 21) shall undergo non-destructive testing as described in subclause 6.5.11.

6.3.1.9 One sample from each batch shall undergo the following:

- a) tightness test;
- b) materials identity test;
- c) visual check for surface appearance;
- d) check for dimensional accuracy.

#### 6.4 Sampling and sample preparation

See figure 1 for location and orientation of test pieces.

#### 6.4.1 Tensile test

6.4.1.1 Tensile test pieces shall be taken parallel to the tube axis in the form of tube sections, flattened strips or round bartest pieces as specified in DIN EN 10 002 Part 1. It shall be permitted to repair local imperfections. The test piece shall not be heat treated nor straightened along its length. Where s exceeds 30 mm, the axis of round bar test pieces shall be located at a point which corresponds to a distance from the outer surface equal to one-fourth of the wall thickness, or as near as possible to this point.

6.4.1.2 In the case of tubes with an outside diameter of 200 mm or more, and where straightening is not required, it shall be permitted to take test pieces transverse to the tube axis and machine them on all sides to produce flat or round bar test pieces.

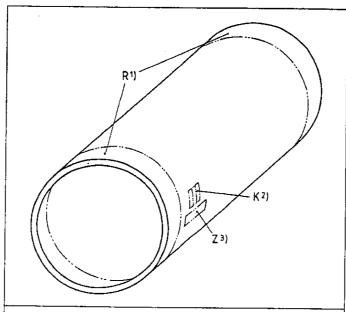
### 6.4.2 Impact test

Where straightening is not required, a set of three ISO-V notch test pieces shall be taken transverse to the tube axis. Otherwise, they shall be taken parallel to the tube axis. Where s exceeds 30 mm, the axis of the test pieces shall be located at a point which corresponds to a distance from the outer surface equal to one-fourth of the wall thickness, or as near as possible to this point.

The test pieces shall be taken and prepared so that the notch axis runs at right angles to the tube surface.

#### 6.4.3 Ring tests

Test pieces for the flattening, expanding ring, drift expanding and ring tensile tests shall be taken from both ends of the sample or the as manufactured length (cf. table 7).



- 1) Cf. subclause 6.4.3.
- Transverse or parallel to tube axis, where s is at least 20 mm (cf. subclause 6.4.2).
- 3) Cf. subclause 6.4.1.

In the above figure,

K = set of three ISO-V notch test pieces as specified in DIN EN 10 045 Part 1;

R = test pieces for ring tests;

Z = tensile test piece.

Figure 1. Test piece location and orientation

Where as manufactured lengths of tube are to be cut to smaller lengths after testing, no further tests need be carried out, provided that the smaller lengths are suitably identified as having been taken from the as manufactured length thus tested.

#### 6.4.4 Chemical composition

For determination of the chemical composition based on a product analysis of the manufactured tube, sample chips shall be taken at points uniformly distributed over the wall thickness, this also applying where spectral analyses are to be carried out. Unless otherwise specified, sampling shall be in accordance with Stahl-Eisen-Prüfblatt 1805.

### 6.5 Test procedure

- 6.5.1 The tensile test shall be carried out at ambient temperature as described in DIN EN 10 002 Part 1.
- 6.5.2 ●● Where it has been agreed to determine the 0,2% and 1% proof stress, testing shall be carried out as described in DIN EN 10 002 Part 5.
- 6.5.3 Impact testing shall be carried out as described in DIN EN 10 045 Part 1.
- **6.5.4** The flattening test shall be carried out as described in DIN 50136, the test pieces or tube ends being flattened until a distance between platens, H, in mm, as defined below, is reached:

$$H = \frac{(1+c)s}{c+s/d_a}$$

where

- s it the wall thickness, in mm;
- $d_a$  is the outside diameter, in mm;
- c is a constant which is equal to 0,10. Where the ratio s/d<sub>a</sub> is greater than 0,25, c shall be reduced by 0,01.
- **6.5.5** The drift expanding test shall be carried out as described in DIN 50135, using a tapered mandrel with a  $60^{\circ}$  taper angle, until the material has expanded, as a function of the ratio inside diameter  $(d_i)$  to outside diameter  $(d_a)$ , by the following amounts (as a percentage of the outside diameter):

20% where  $d_i/d_a$  is greater than 0,6; 15% where  $d_i/d_a$  is less than or equal to 0,6.

- **6.5.6** The expanding ring test shall be carried out as described in DIN 50 137. Test pieces shall be subjected to load until fracture, or until the inside diameter has expanded to 40%, then assessed.
- 6.5.7 The ring tensile test shall be carried out as described in DIN 50138.
- 6.5.8 The chemical composition shall be tested using a method specified in the *Handbuch für das Eisenhüttenlaboratorium* (Handbook for the ferrous metallurgy laboratory) and developed by the Chemists' Committee of the *Verein Deutscher Eisenhüttenleute* (Society of German Ferrous Metallurgy Engineers).
- 6.5.9 Tightness testing shall be carried out by applying an internal hydrostatic pressure as described in DIN 50104. Unless otherwise agreed, the test pressure shall be 80 bar and maintained for at least five seconds.

The load level shall not be below a value corresponding to 1,1 times the factor of safety with respect to the 0,2% proof stress (cf. subclause 4.6 of the June 1972 edition of DIN 2413, where this factor is equal to 0,9). This shall also be considered when testing thin-walled tubes with large outside diameters at 80 bar.

Where tightness testing is carried out with air and with a foaming medium, the test pressure shall be 0,3 bar and maintained for at least five seconds.

- •• Unless otherwise specified, the manufacturer shall select one of the above methods for tightness testing. Instead of internal hydrostatic pressure testing, non-destructive testing (e.g. eddy current testing as described in Stahl-Eisen-Prüfblatt 1925) or tightness testing using helium may be carried out.
- **6.5.10** Non-destructive testing of the tube ends shall be carried out as described in Stahl-Eisen-Prüfblatt 1919, where s exceeds 40 mm. This may also be carried out, instead of the ring tensile test, where s is not more than 40 mm and an outside diameter exceeding 508 mm.
- **6.5.11** When tubes with an outside diameter exceeding 20 mm and a wall thickness exceeding 2 mm are checked for longitudinal imperfections by ultrasonic testing, the requirements given in *Stahl-Eisen-Prüfblatt* (Iron and steel test sheet) 1915 shall be met.
- 6.5.12 ●● If so agreed, tubes may be subjected to ultrasonic testing for longitudinal imperfections as described in Stahl-Eisen-Prüfblatt 1915 or for transverse imperfections as described in Stahl-Eisen-Prüfblatt 1918, with the exception of tubes made from material number 1.4959.
- 6.5.13 ●● If so agreed, tubes made from material number1.4959 may be subjected to ultrasonic testing.
- 6.5.14 ●● If so agreed, tubes with an outside diameter not exceeding 20 mm and a wall thickness not exceeding 2 mm shall be subjected to ultrasonic testing as described in Stahl-Eisen-Prüfblatt 1915.
- **6.5.15** A visual check of the outside and, as far as possible, the inside of tubes, shall be made by a person with normal vision under sufficient light.
- Note. Instead of the visual check, the manufacturer and purchaser may agree on a suitable alternative method.
- **6.5.16** Tube dimensions shall be measured using suitable instruments.
- 6.5.17 Determination of straightness shall be carried out by suitable means.
- 6.5.18 Determination of materials identity shall be carried out by suitable means (e.g. spectroscopy).

#### 6.6 Retests

- **6.6.1** Tubes which do not pass the tests specified in subclauses 6.5.4 to 6.5.17 (except for subclause 6.5.8) shall be sorted out. The manufacturer shall be entitled to correct any defects or deficiencies determined upon testing and to submit the tubes for renewed inspection.
- 6.6.2 If one test tube fails the tensile test or the impact test, the manufacturer shall be permitted to retest twice the number of test pieces taken from the same tube, in which case all test pieces shall satisfy the requirements. If this is not the case, the tube shall be sorted out.

Instead of retesting the failed tube as described above, two other tubes may be taken from the same batch and subjected to renewed tensile and impact testing. Should these tubes also fail, the batch shall be deemed not to be in conformance with the standard. However, the manufacturer and purchaser may agree that all units belonging to the same batch be tested individually.

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analysis 1
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composition as
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Table 1.

Material							Percer	Percentage by mass			
designation	number	U	ï	Ā	а	s	Z	٥	Mo	Ä	Others
,					тах.	тах.					
X 6 CrNi 18 11	1.4948	0,04 to 0,08	57,0≥	≥ 2,0	0,035	0,015		17,0 to 19,0		10,0 to 12,0	
X 3 C7NIN 1811	1.4949	≥ 0,04	≤ 0,75	≤ 2,0	0,035 0,015	0,015	0,10 to 0,18	17,0 to 19,0	0,20 to 0,50	9,5 to 11,5	
X 8 CrNTTI 1810	1.4941	0,04 to 0,10	≤ 0,75	≤ 2,0	0,035 0,015	0,015		17,0 to 18,5	09'0 ⋝	9,5 to 11,5	Ti: ≥ 5 × %C to ≤ 0,80
									•		B: 0,0015 to 0,0050
X 6 CrNiMo 1713	1.4919	0,04 to 0,08	≤ 0,75	≤ 2,0	≤ 2,0 0,035 0,015	0,015		16,0 to 18,0	2,0 to 2,5	12,0 to 14,0	
X 3 CrNIMON 17 13	1,4910	≥ 0,04	< 0,75	≤ 2,0	≤ 2,0 0,035 0,015	0,015	0,10 to 0,18	16,0 to 18,0	2,0 to 2,8	12,0 to 14,0	B: 0,0015 to 0,0050
X 8 CrNIND 1613	1.4961	0,04 to 0,10	0,30 to 0,60	≤ 1,5	0,035	0,015		15,0 to 17,0	,	12,0 to 14,0	Nb: $\geq 10 \times \%C \text{ to } \leq 1,2^2$ )
X 8 CrNIMoNb 1616	1.4981	0,04 to 0,10	0,30 to 0,60	≤ 1,5	< 1,5 0,035 0,015	0,015		15,5 to 17,5	1,6 to 2,0	15,5 to 17,5	Nb: ≥ 10 × %C to ≤ 1,22)
X 8 CrNIMo VNb 1613 1.4988	1.4988	0,04 to 0,10	0,30 to 0,60	< 1,5	< 1,5 0,035 0,015		0,06 to 0,14	15,5 to 17,5	1,10 to 1,50	12,5 to 14,5	'Nb: ≥ 10 × %C to ≤ 1,22)
						-					V: 0,60 to 0,85
X 5 NICrAITI 31 20	1.4958	0,03 to 0,08	0,70 ≥	≥ 1,5	0,015	0,010	The state of the s	19,0 to 22,0		30,0 to 32,5	Al: 0,20 to 0,50
										-	Ti: 0,20 to 0,50
											(Al + Ti): ≤ 0,70
									•		. Co: ≤ 0,5
											(Ni + Co): 30,0 to 32,5
			-				,				Cu: ≤ 0,5
											Nb: ≤ 0,1
X 8 NICrAITI 32 21	1,4959	0,05 to 0,10	0,70 ≥	5,1,5	0,015 0,010	0,010		19,0 to 22,0		30,0 to 34,0	At: 0,25 to 0,65
•								•			Ti: 0,25 to 0,65
										- <del>-</del>	Co: ≤ 0,5
							<del>,</del>				(Ni + Co): 30,0 to 34,0
							<del></del>				Cu: ≤ 0,5
				] .	1	1					

1) Any elements for which values have not been specified may be present, provided the properties of the steel and its weldability are not adversely affected.
2) The content specified represents niobium and tantalum together.

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Table 2. Amounts by which the chemical composition as determined by product analysis may deviate from the limiting values specified for ladie analysis

Element	Maximum content as determined by ladle analysis, as a percentage by mass	Limit deviations in the product analysis from the limiting values specified for the ladle analysis, as a percentage by mass 1)
C .	≤ 0,04 > 0,04 to ≤ 0,10	+ 0,01 ± 0,01
Si	≤ 0,75	± 0,05
Mn	≤ 2,0	+ 0,04
Р	≤ 0,035	+ 0,005
s	≤ 0,010 > 0,010 to ≤ 0,015	+ 0,003 + 0,005
N	≤ 0,18	± 0,01
Αl	≥ 0,20 to ≤ 0,75	± 0,05
В	≥ 0,0015 to ≤ 0,0050	± 0,0005
Co	≤ 0,5	+ 0,05
Cr	≥ 15,0 to ≤ 22,0	± 0,20
Cu	≤ 0,5	+ 0,05
Мо	$\geq$ 0,20 to $\leq$ 0,60 > 0,60 to $\leq$ 2,0 > 2,0 to $\leq$ 2,8	± 0,03 ± 0,05 ± 0,10
NI	≥ 9.5 to ≤ 20.0 > 20.0 to ≤ 34.0	± 0,15 ± 0,20
Nb	≤ 1,20	± 0,05
Ti	≤ 0,80 :	± 0,05
V	≥ 0,60 to ≤ 0,85	± 0,03

<sup>1)</sup> If a number of product analyses are to be carried out, the deviations within one cast that an element shows shall either be above the upper limit or below the lower limit of the range specified for the ladie analysis, but not both at the same time for one cast.

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Table 3. Mechanical properties of tubes with wall thicknesses up to 50 mm 1), at ambient temperature

							•		
Material		Heat treatment condition	Min. 0,2 % proof stress,	1 '	Tensile strength, in N/mm <sup>2</sup>	at frac $(L_0 = 5)$	ongation ture, $A_5$ ,65 $\sqrt{S_0}$ ), s a entage	Min. i ene	mpact rgy <sup>2</sup> ) V), in J
designation	number		in N/mm <sup>2</sup>	in N/mm <sup>2</sup>		Lon- gitu- dinal	Trans- verse	Lon- gitu- dinal	Trans- verse
X 6 CrNi 1811	1.4948	Solution heat treated	185	225	500 to 700	40	30	90	60
X 3 CrNIN 1811	1.4949	Solution heat treated	240.	275	500 to 700	35	30	90	60
X 8 CrNiTi 1810 <sup>3</sup> )	1.4941	Solution heat treated	195	235	490 to 640	35	30	90	60
X 6 CrNiMo 1713 1.4919		Solution heat treated	205	245	490 to 690	35	30	90	60
X 3 CrNiMoN 1713	1.4910	Solution heat treated	260	300	550 to 750	35	30	120	80
X 8 CrNINb 1613	1.4961	Solution heat treated	205	245	510 to 690	.35	22	65	45
X 8 CrNIMoNb 16164)	1.4981	Solution heat treated	215	255	530 to 690	35	22	65	45
X 8 CrNIMoVNb 16134)	1.4988	Solution heat treated and aged	255	295	540 to 740	30	20	50	35
X 5 NiCrALTI 31 20 RK	1.4958 RK	Annealed for recrystallization	210	240	500 to 750	35	30	120	80
X 5 NICIALTI 3120	1.4958	Solution heat treated	170	200	500 to 750	35	30	120	80
X 8 NICrALTI 3221	1.4959	Solution heat treated	170	200	500 to 750	· 35	30	120	80

- 1) Where the wall thickness exceeds 50 mm, values of mechanical properties shall be the subject of agreement.
- 2) Represents the mean from three test pieces. One single value may be lower, by not more than 30 %.
- 3) Values apply to cold formed tubes; in the case of hot formed tubes, the values shall be the subject of agreement.
- 4) Values apply to tubes with an outside diameter up to 20 mm.
- 6.6.3 The manufacturer shall be permitted to correct defects or deficiencies by means of heat treatment or in another suitable manner, and resubmission of a failed batch shall be at his discretion. If the batch fails testing after resubmission, it shall be deemed not to be in conformance with this standard.
- 6.6.4 Test results that may be deemed to have been falsified by incorrect sampling, sample preparation or testing shall not be counted.

### 7 Marking

- 7.1 One end of each tube in compliance with this standard shall be clearly and durably marked with the following information:
- a) manufacturer's mark;
- b) material designation or number;
- c) symbol denoting heat treatment condition (cf. table 5);
- d) the letter 'X', where tubes made from grade X 8 CrNITi 18 10 have been hot formed;
- e) article number and, where the outside diameter is 114,3 mm or more, the symbol denoting cast number, or the number itself:

- f) the inspector's mark;
- g) symbol indicating that non-destructive testing in accordance with subclause 6.5.12 has been carried out.
- 7.2 Tubes shall be marked by means of stamping, engraving or imprinting. Thin-walled tubes or those with a small outside diameter may be marked by other suitable means (e.g. by labelling the bundle).
- 7.3 •• Continuous marking of a length of tube may be agreed at the time of ordering.

### 8 Complaints

- 8.1 Under current law, warranty claims may only be raised against defective products if the defects impair their processing and use to a more than negligible degree. This shall apply unless otherwise agreed at the time of ordering.
- 8.2 It is normal and practical for the purchaser to give the supplier the opportunity to judge whether the complaints are justified, if possible by submitting the products objected to or samples of the products supplied.

Table 4. Minimum values of elevated temperature 0,2% and 1% proof stress

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Material	-	Heat treatment	0.2	% proo	f stress, tempi	0,2% proof stress, in N/mm², at the following temperatures, in °C	m², at th , in °C	e follow	ing	- T	e proof	stress, i	ress, in N/mm², at themperatures, in °C	1% proof stress, in N/mm², at the following temperatures, in °C	• followi	Đ <sub>L</sub>
designation	number		001	200	300	400	200	550	009	100	200	300	400	200	550	009
X 6 CrNi 18 11	1.4948	Solution heat treated	157	127	108	98	. 88	83	7.8	191	157	137	127	118	113	108
X 3 CrNIN 1811	1.4949	Solution heat treated	185	150	130	120	110	105	100	220	175	150	140	130	125	120
X 8 CrNITI 1810 1)	1.4941	Solution heat treated	162	142	132	123	113	108	103	201	181	172	162	152	147	142
X 6 CrNIMo 1713	1,4919	Solution heat treated	177	147	127	118	108	103	86	211	177	157	147	137	132	128
X 3 CrNIMoN 1713	1.4910	Solution heat treated	205	170	148	134	127	124	121	240	200	178	164	157	154	151
X 8 CrNINb 1613	1.4961	Solution heat treated	175	157	137	128	118	118	113	205	186	167	157	147	147	142
X 8 CrNIMoNb 1616	1.4981	Solution heat treated	195	177	157	147	137	137	132	225	206	186	171	167	167	162
X 8 CrNIMoVNb 1613	1,4988	Solution heat treated and aged	215	196	177	167	157	152	147	245	226	206	196	186	181	177
X 5 NICFALTI 3120 RK	1.4958RK	Annealed for recrystallization	180	160	145	130	120	115	110	205	180	165	155	145	140	135
X 5 NICFALTI 3120	1.4958	Solution heat treated	140	115	95	85	80	75	75	160	135	115	105	9	96	95
X 8 NICralti 3221	1.4959	Solution heat treated	140	115	95	85	08	7.5	75	160	135	115	105	001	95	95
				1				-	-				_			

1) Values apply to cold formed tubes; in the case of hot formed tubes, the values shall be the subject of agreement.

Table 5. Heat treatment condition and surface quality

Symbol	Heat treatment condition	Surface quality
c1 or II a	Hot formed, heat treated 1), descaled	
c2 or II a	Hot formed, heat treated 1), pickled	Clean
h or III b	Cold formed, heat treated, pickled	Pickled bright, smoother than condition c2 (II a)
m or III d	Cold formed and heat treated (scale-free)	Bright annealed, smoother than condition h (III b)

Table 6. Summary of scope of testing and DIN 50 049 (EN 10 204) inspection documents (See figure 1 for location and orientation of test pieces and subclause 6.3.1 for batch sizes.)

	Test to be carried	out		
No.		Subclause	Scope of testing	DIN 50 049 inspection document
1	Ladle analysis	5.3.1	1 analysis per cast or casting unit (all elements given in table 1 for the relevant grade)	EN 10 204 inspection report
2	Tensile test at ambient temperature	6.3.1.2 6.4.1 6.5.1	1 test piece from one sample per batch 1)	EN 10204 inspection report or certificate A, B or C
3	Impact test	6.3.1.2 6.4.2 6.5.3	1 set of 3 test pieces from 1 sample per batch, where s is at least 20 mm <sup>2</sup> )	EN 10 204 inspection report or certificate A, B or C
4	Ring test (cf. table 7)	6.3.1.5 6.4.3 6.5.4 6.5.5 6.5.6 6.5.7	1 test piece from one end of each tube or as manufactured length, where s does not exceed 40 mm <sup>3</sup> )	EN 10 204 inspection report or certificate A, B or C
5	Non-destructive testing of tube ends	6.3.1.6 6.5.10	All tubes, where s exceeds 40 mm.	EN 10 204 inspection certifcate B
6	Tightness test	6.3.1.9 6.5.9	All tubes	EN 10 204 inspection certificate B
7	Visual check	6.3.1.9 6.5.15	All tubes	EN 10 204 inspection report or certificate A, B or C
8	Materials identity test	6.3.1.9 6.5.18	All tubes	EN 10 204 inspection certificate B
9	Check for dimensional accuracy	6.3.1.9 6.5.16 6.5.17	All tubes	EN 10 204 inspection report or certificate A, B or C
10	Non-destructive testing of tube 4)	6.3.1.6 6.5.11	All tubes	EN 10 204 inspection certificate B
1	•• Tensile test at elevated temperature	6.3.1.2 6.5.2	Subject to agreement.	EN 10 204 inspection report or certificate A, B or C
12	●● Product analysis	6.4.4 6.5.8	1 analysis per cast.	EN 10 204 inspection certificate B

<sup>1)</sup> Where tubes with an outside diameter of 200 mm or more and a wall thickness of 12 mm or more are to be used as pressure vessel shells, test pieces shall be taken from 10% of the tubes per batch.

<sup>2)</sup> Where tubes are to be used as pressure vessel shells, test pieces shall be taken from 10% of the tubes per batch.

<sup>3)</sup> Where tubes are to undergo ultrasonic testing as described in Stahl-Eisen-Prüfblatt 1915 and 1918, test pieces shall be taken from 10% of the tubes per batch.

<sup>4) ••</sup> Subject to agreement in the case of tubes with an outside diameter not exceeding 20 mm and a wall thickness not exceeding 2 mm and of tubes made from grade X 8 NiCrAITi 32 21 (cf. subclause 6.5.12).

Table 7. Ring tests to be carried out (as a function of tube size)

Tube diameter,	In mm		Wall thickness, in mm	
Outside	Inside	Up to 2	Over 2 up to 16	Over 16 up to 40
≤ 21,3	≤ 15	Flattening test	Flattening test	-
≤ 21,3	> 15	Flattening test	Expanding ring test 1)	<del>-</del>
> 21,3 ≤ 146	≤ 15		Expanding ring test 1)	Flattening test
> 21,3 ≤ 146	> 15	Flattening test		Flattening test
> 146	≤ 100		Ring tensile test 2)	Ring tensile test
> 146	> 100		-	Ring tensile test

<sup>1)</sup> A drift expanding test may be performed instead of the expanding ring test.

### Appendix A

### Additional information

#### A.1 Rupture stress

Table A.1 specifies guideline values for the rupture stress of seamless tubes as covered here. The values represent mean values from scatterbands established to date and may be revised at a later date, as investigations continue. According to current data, it may be assumed that the lower limit of the scatterband is approximately 20% lower than the mean value specified.

The scatterband is greater for X 5 NiCrAITi 31 20 RK steel at temperatures over 550 °C and for X 8 NiCrAITi 32 21 steel at temperatures over 700 °C. In the case of the former steel, the lower limit of the scatterband is lower than the mean values specified by the following amounts:

approx. 20% at 550°C;

approx. 25% at 600°C;

approx. 30 % at 700 °C.

In the case of the latter steel, it is lower by the following amounts:

approx. 20 % at 700 °C:

approx. 25 % at 800 °C:

approx. 30 % at 900 °C;

approx. 35 % at 1000 °C.

### A.2 Guideline values for physical properties

Selected guideline values for physical properties are given in table A.2 and have been taken from Stahl-Eisen-Werk-stoffblatt (Iron and steel materials sheet) 310 (at present at the stage of draft), issued by the Verein Deutscher Eisenhüttenleute, Postfach 82 09, D-4000 Düsseldorf 1.

# A.3 Guideline temperatures for heat treatment and hot forming

A.3.1 Table A.3 gives guideline temperatures for heat treatment and hot forming.

A.3.2 Although the steels covered here are usually suitable for cold forming, it should be noted that this will alter their mechanical and physical properties.

### A.4 Additional information on heat resistance

In addition to the specifications given in table 4, information on the heat resistance of X 5 NiCrAlTi 31 20 and X 8 NiCrAlTi 32 21 steels is provided in table A.4, which is based on tensile tests at elevated temperature, a rate of strain of 0.5% per minute having been applied.

<sup>2)</sup> Instead of the ring tensile test, the manufacturer shall be permitted to perform non-destructive testing as described in subclause 6.5.10 in the case of tubes with an outside diameter exceeding 508 mm.

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Table A.1. Guideline values for rupture stress

Material	ı	Heat treatment	Temper- ature, in		ep limit 1), m², after	Re ii	upture stres: n N/mm², aft	s <sup>1</sup> ), er
designation	number	condition	°C	10 000 h	100 000 h	10 000 h	100 000 h	200 000 r
X 6 CrNi 18 11	1.4948	Solution heat treated	500 510 520 530 540	147 142 137 132 127	114 111 108 104 100	250 239 227 215 203	192 182 172 162 151	176 166 156 146 136
			550 560 570 580 590	121 116 111 106 100	96 92 88 84 79	191 177 165 154 143	140 128 117 107 98	125 114 104 95 86
			600 610 620 630 640	94 88 82 75 68	74 69 63 56 49	132 122 113 104 95	89 81 73 65 58	78 70 62 55 49
			650 660 670 680 690	61 55 49 44 39	43 37 32 28 25	87 80 73 67 61	52 47 42 37 32	43 38 34 30 26
			700 710 720 730 740	35 (31) (28) (26) (25)	22 (15) (14) (13) (12)	55 (45) (41) (38) (36)	28 (22) (20) (18) (16)	22
X 3 CrNIN 18 11			750	(24)	(11)	(34)	(15)	
	1.4949	Solution heat treated	550 560 570 580 590			230 216 202 188 174	178 163 150 137 125	
			600 610 620 630 640			160 146 133 121 110	114 103 92 82 73	
			650 660 670 680 690			100 91 82 74 67	64 56 49 42 36	
			700			60	30	
X 8 CrNITi 18 10	1.4941	Solution heat treated	550 560 570 580 590			230 220 210 190 170	170 150 140 120 110	150 130 120 110 100
			600 610 620 630 640			160 140 130 120 110	100 92 84 76 68	90 82 74 66 60

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Table A.1 (continued).

Material		Heat treatment	Temper- ature, in	1 % cre	eep limit, m², after	Ru	upture stres: n N/mm², afi	s ¹), ter
designation	number	condition	°C	10 000 h	100 000 h	10 000 h	100 000 h	200 000 h
X 8 CrNiTi 18 10 (concluded)	1.4941	Solution heat treated	650 660 670 680 690			100 90 82 74 66	62 56 50 44 39	54 48 43 40 38
X 6 CrNiMo 17 13	4 4045		700	<del> </del>		60	35	29
NO SINIMO 17 13	1.4919	Solution heat treated	550 560 570 580 590	180 169 158 147 136	125 117 109 101 93	250 235 220 205 190	175 164 153 142 131	
			600 610 620 630 640	125 115 105 96 87	85 77 70 63 56	175 160 147 135 123	120 109 98 88 78	
			650 660 670 680 690	79 71 64 57 51	49 43 38 33 29	111 100 91 82 73	69 60 52 46 40	
0.0.1			700	46	25	65	34	
3 Crnimon 1713	1.4910	Solution heat treated	550 560 570 580 590			290 272 254 237 220	220 202 186 170 155	(200) (184) (166) (151) (137)
			600 610 620 630 640			205 190 174 162 148	141 127 114 102 92	(122) (113) (100) (91) (81)
			650 660 670 .680 690			135 122 112 102 93	83 75 68 61 56	(73) (65) (58) (52) (46)
			700 710 720 730 740			84 78 71 65 58	52 48 45 41 37	(42) (39) (36) (34) (31)
			750 760 770 780 790			52 48 44 41 37	34 31 28 25 22	(28) (26) (24) (21) (19)
CrNiNb 1613			800			33	20	(17)
CHAMP 10 13	h	olution eat reated	580 590	127 120	91 84	182 170	129 119	115 105
		Caley	600 610 620 630 640	113 106 99 92 85	78 73 67 61 55	157 145 134 124	108 98 89 80	94 85 77 69

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Table A.1 (continued).

Material	1	Heat treatment	Temper- ature, in	1 % cree	ep limit <sup>1</sup> ), m <sup>2</sup> , after	. Ri	upture stres: n N/mm², aft	s <sup>1</sup> ), ter
designation	number	condition	°C	10 000 h	100 000 h	10 000 h	100 000 h	200.000
X 8 CrNINb 1613 (concluded)	1.4961	Solution heat treated	650 660 670 680 690	78 72 66 59 54	49 44 39 34 30	103 93 84 76 70	64 57 50 44 39	53 47 41 36 31
			700 710 720 730 740	49 45 42 39 36	26 24 21 19 17	64 59 55 51 47	34 30 27 25 22	27 25 22 19 17
			750	34	16	44	20	15
(8 CrNiMoNb 1616	1.4981	Solution heat treated	580 590	177 167	128 118	270 246	186 169	162 147
er.			600 610 620 630 640	157 147 137 128 118	108 98 88 79 72	225 205 186 169 152	152 136 122 107 94	132 118 103 91 80
			650 660 670 680 690	108 98 89 80 72	64 56 49 43 38	137 124 111 100 91	83 75 66 59 51	71 63 55 49 42
			700 710 720 730 740	64 58 53 47 44	34 29 26 22 19	83 77 70 64 59	44 37 31 26 23	35 29 24 20 17
X 8 CrNiMoVNb 1613			750	42	17	54	20	15
8 CrNiMoVNb 1613	1.4988	Solution heat treated and aged	580 590	202 194	152 145	299 274	209 189	180 164
		and aged	600 610 620 630 640	186 176 165 152 139	137 128 117 106 95	250 228 207 189 173	172 156 139 125	147 132 117 105 93
5 NG-4177 04 50 514	-		650	128	83	157	98	82
5 NICFALTI 3120 RK	1.4958 RK	Annealed for recrys- tallization	500 510 520 530 540			315 297 280 262 243	258 241 224 206 189	(242) (225) (207) (190) (172)
			550 560 570 580 590	164 154 144 133 123	(132) (122) (111) (101) (92)	224 204 184 165 147	171 153 136 119 104	(155) (138) (122) (106) (92)
			600 610 620 630 640	113 103 93 84 75	(82) (74) (65) (58) (51)	131 117 106 96 87	90 79 70 62 56	(80) (70) (62) (55) (49)

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Table A.1 (concluded).

Material	1	Heat	Temper- ature, in	In Nit-	ep limit 1), m², after	A A	upture stres n N/mm², af	s <sup>1</sup> ), ter
designation	number	condition	°C	10 000 h	100 000 h	10 000 h	100 000 h	200 000 h
X5 NICrALTI 31 20 RK (concluded)	1.4958 RK	Annealed for recrys- tallization	650 660 670 680 690	67 60 55 50 45	(46) (41) (37) (33) (30)	80 73 67 61 55	51 46 42 38 34	(44) (40) (36) (33) (29)
X5 NICIALTI 31 20	1.4958	0-1-4	700	41	(27)	50	30	(26)
	1.4936	Solution heat treated	500 510 520 530 540			290 279 267 254 240	215 205 195 184 172	(196) (186) (176) (166) (155)
			550 560 570 580 590			225 208 190 172 155	160 147 133 119 106	(143) (130) (117) (105) (93)
			600 610 620 630 640	115 109 102 96 90	(85) (79) (74) (69) (64)	140 128 118 109 103	95 85 78 72 67	(83) (74) (68) (63) (59)
			650 660 670 680 690	84 78 73 68 63	(59) (55) (51) (47) (43)	97 91 85 80 74	63 59 55 52 48	(55) (52) (48) (45) (41)
(8 NICrA(T) 32 21	1.4959	C-ludi-	700	58	(40)	69	44	(38)
		Solution heat treated (at 1100 to 1200 °C)	700 710 720 730 740	59,0 55,5 52,0 48,5 45,0	42,0 38,0 34,4 31,3 28,4	74,0 68,0 62,0 56,0 51,5	50,0 45,0 40,9 37,4 34,3	(44,0) (39,4) (35,5) (32,2) (29,3)
			750 760 770 780 790	41,7 38,4 35,6 32,9 30,5	26,0 23,5 21,3 19,3 17,6	47,5 43,7 40,5 37,5 35,0	31,6 29,1 27,0 24,9 23,1	(26,8) (24,6) (22,4) (20,7) (19,0)
			800 810 820 830 840	28,2 26,2 24,2 22,4 20,8	16,0 14,7 13,4 12,1 11,1	32,6 30,4 28,4 26,5 24,7	21,4 19,8 18,4 17,0 15,7	(17,5) (16,2) (15,1) (14,0) (13,0)
			850 860 870 880 890	19.1 17,6 16.1 14,7 13,4	10,0 9,1 8,2 7,3 6,5	23.0 21,4 19,9 18,4 17,0	14,4 13,3 12,2 11,2 10,3	(12,1) (11,2) (10,3) (9,5) (8,7)
			900 910 920 930 940	12,1 10,9 9,8 8,8 7,8	5,7 5,0 4,4 3,9 3,4	15,6 14,4 13,2 12,1 11,1	9,4 8,6 7,8 7,1 6,4	(8,0) (7,3) (6,7) (6,2) (5,6)
			950 960 970 980 990 1000	6,9 6,1 5,3 4,6 4,0 3,5	2,9 2,5 2,1 1,8 1,6 1,4	10.1 9,2 8,4 7,7 7,0 6,4	5,8 5,3 4,8 4,4 4,0	(5,0) (4,5) (4,1) (3,7) (1,3)

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Material		Density,	<u> </u>	ž	odutus	Modulus of elasticity, in $10^9~N/m^2$ , at a temperature, in $^{\circ}$ C, of	Hicity, ir	1 10 <sup>9</sup> N	/m², at	a tem	peratun	es		్రి	efficie	Coefficient of linear thermal expansion, in 10-5 · K-1, at a temperature between 20 °C and	near th	ermal e	xpansit	n, in 18	. ¥. −		Thermal conductance,	Specific heat capacity,	Resistivity,
designation	питрег	III III KRAMI	8	8	200	300	480	200	969	- DEZ		906	1000	100	200	300 40	400	200   200	00 / 700	0 800	- 300	961	in W/(m·K). at 20°C	in J/(kg·K). at 20°C	at 20°C
X 6 ErNi 18 11	1.4948										<u> </u>			<del> </del>			<del> </del> -	├			<del> </del>				
X3 Crnin 18 11	1.4949	7,93							· · · · · ·			<del></del>							<del></del> .		<del></del> -		4		0,71
X 8 Cr NITI 18 10	1.4941							<del>-</del> · . <u>-</u> -			· <del>-</del>				<del>-</del>	·		<del></del> -		<u> </u>	·				
X 6 CFNIMo 1713	1.4919	80 %		Ę	Ę						<del>-</del>														
X 3 Grrimon 17 13	1.4910	D	8	761	3	2	<u> </u>	FC .	 B	142		· · · · · ·	<del>=</del>	6,3	16.9	17,8	19,2	18,5	18,7	~			:	450	0,77
X 8 CFNING 16 13	1.4961	7,98		-			<del>- · · · · · · · · · · · · · · · · · · ·</del>					<del></del>				· · · · ·		<del></del>					<b>=</b>		82,0
X 8 Crnimond 16 16	1.4981	8,01							<del></del> _							<del></del>								_!	7,00
X 8 CrNIMoVNh 1613	1.4988	7,95					<del></del>				<del></del> -							·	-		<u>.                                    </u>		52		0.79
X 5 NICralti 31 20 RK	1.4958 RK									<del> </del>			<del> </del> -	<del> </del>	ļ. <u> </u>		<u> </u>		<del> </del>	<u> </u>					
X 5 NIGIALTI 31 20	1.4958	7,94	197	191	184	#		162	155 1,	148	141	134 12	127 15,4	4 16,0	16,5	5 16,8	17,2	17,5	17.9	18,3	18,6	19,0	12	460	86'0
X B NICralti 32 21	1.4959						·	<del>-</del> ·			· ·					·- <u>-</u>									<u>.</u>
1) Cf. [1].									<del> </del>	-	1 1	-	]	-		-	<u> </u>	1	_						

Table A.2. Guideline values for physical properties 1)

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Table A.3. Guideline temperatures for heat treatment and hot forming

Material	ŧ	Temperatur	re, in °C, for	Hot fo	rming
designation	number	annealing for recrystallization 1)	solution heat treatment 1)	Temperature, in °C	Quenching
X 6 CrNI 1811	1.4948	-	1000 to 1080		medium
X 3 CrNIN 18 11	1.4949	_	1000 to 1080		
X8 CrNiTI 1810	1.4941	-	1070 to 1150		
X 6 CrNIMo 1713	1.4919	_	1020 to 1100		
X3 CrNIMoN 1713	1.4910	_	1020 to 1100	1150 to 750	Air
X 8 CrNINb 1613	1.4961	_	1050 to 1100		7.11
X 8 CrNiMoNb 1616	1.4981	_	1050 to 1100		
X 8 CrNiMoVNb 1613	1.4988		1100 to 1150 <sup>2</sup> )		
K 5 NiCrALTI 31 20	1.4958	920 to 1000	1100 to 1200		
(8 NICrALTI 32 21	1.4959		1100 to 1200 <sup>3</sup> )		

<sup>1)</sup> Followed by rapid quenching in water or air.

Table A.4. 0,2% proof stress at temperatures over 600  $^{\circ}\text{C}$ 

Material		Heat treatment	Minimur ai	m 0,2 proof t a tempera	stress 1), in	1 N/mm²
designation	number	condition	700	800	900	1
X 5 NICrALTI 31 20	1.4958	Solution heat treated	<del></del>		300	1000
X 8 NICIALTI 32 21	1.4959	Solution heat treated	75	70	50	20

<sup>1)</sup> The values are based on tensile tests at elevated temperature, a rate of strain of 0,5% per minute having been

# Standards and other documents referred to

	and documents referred to
DIN 2413	Design of wall thickness of steel tubes for resistance to internal pressure
DIN 2462 Part 1	Seamless stainless steel tubes directions to internal pressure
DIN 8528 Part 1	Seamless stainless steel tubes; dimensions and mass per unit length Weldability of metallic materials; concepts
DIN 8556 Part 1	Esta materials; concepts
	Filler metals for welding stainless and heat resisting steel; designation and technical delivery condi-
DIN 17014 Part 1	Heat treatment of ferrous materials; terminology
DIN 50 049	Inspection decompositions inderrais; terminology
DIN 50 104	Inspection documents for the delivery of metallic materials
DIN 50 135	Internal hydrostatic pressure testing of hollow bodies; general specifications
	or metal tubes
DIN 50 136	Flattening test on metal tubes
DIN 50 137	Expanding ring test on metal tubes
DIN 50 138	Ring tensile test on metal tubes
DIN EN 10 002 Part 1	Tensile testing of motal tages
DIN EN 10 002 Part 5	Tensile testing of metallic materials; method of test at ambient temperature
DIN EN 10 045 Part 1	resisting of metallic materials; method of test at elevated temperatures
2.11 211 10 045 Part 1	Metallic materials; Charpy notched bar impact test; method of test

 $<sup>^2)</sup>$  Followed by ageing at 750 to 800  $^{\circ}\text{C}$  for 1 to 5 h in air.

<sup>3)</sup> After solution heat treatment, the grain size index shall be within the range of 1 to 5 as specified in EURONORM 103.

#

### Page 18 DIN 17459

**EURONORM 103** 

Microscopic determination of the ferritic and austenitic grain size of steel

Stahl-Eisen-Prüfblatt 1805 Probenahme und Probenvorbereitung für die Stückanalyse bei Stählen (Sampling and sample preparation for the product analysis of steel)\*)

Stahl-Eisen-Prüfblatt 1915 Ultraschallprüfung auf Längsfehler von Rohren aus warmfesten Stählen (Ultrasonic testing for longitudinal imperfections in steel tubes with elevated temperature properties)\*)

Stahl-Eisen-Prüfblatt 1918 Ultraschallprüfung auf Querfehler von Rohren aus warmfesten Stählen (Ultrasonic testing for transverse imperfections in steel tubes with elevated temperature properties)\*)

Stahl-Eisen-Prüfblatt 1919 Ultraschallprüfung auf Dopplungen von Rohren aus warmfesten Stählen (Ultrasonic testing for laminations in steel tubes with elevated temperature properties)\*)

Stahl-Eisen-Prüfblatt 1925 Elektromagnetische Prüfung von Rohren zum Nachweis der Dichtheit (Electromagnetic testing of tubes for verification of leak tightness)\*)

Handbuch für das Eisenhüttenlaboratorium\*)

### Literature

[1] F. Richter, Physikalische Eigenschaften von Stählen und ihre Temperaturabhängigkeit (Physical properties of steel as a function of temperature), published in Stahl-Eisen-Sonderberichte (Iron and steel special reports), 1983: 10\*).

### **Explanatory notes**

Some of the steel grades specified here have been taken from Stahl-Eisen-Werkstoffblatt (SEW) 670 and Stahl-Eisen-Lieferbedingungen (Iron and steel delivery conditions) (SEL) 675, which have been withdrawn.

Up to now, steel grades X 8 CrNiNb 16 13, X 8 CrNiMoNb 16 16 and X 8 CrNiMoVNb 1613 were supplied on the basis of SEW 670, SEL 675 and of VdTÜV-Werkstoffblatt (VdTÜV Materials sheet) 1041).

Steel grades X 6 CrNiMo 1713 and X 6 CrNi 18 11, as specified in VdTÜV-Werkstoffblätter 312 and 313 respectively, have been available for a long time, but were not covered in SEW 670.

Steel grades X 3 CrNiN 18 11 and X 3 CrNiMoN 17 13, as specified in VdTÜV-Werkstoffblätter 383 and 484 respectively, are relatively new materials, information regarding the good performance of the latter grade having already been published.

Requirements regarding grade X 8 CrNiTi 18 10 are based on experience gathered with the high-temperature steel with material number 1.4878 as specified in SEW 470 and the influence of molybdenum on the strength of that steel. The chemical composition specified for steel grade X 8 CrNiTi 18 10 is largely in compliance with the information given in VdTÜV-Werkstoffblatt 464.

Grades X 5 NiCrAlTi 31 20 and X 8 NiCrAlTi 32 21 are variants of the high-temperature steel grade X 10 NiCrAlTi 32 20 (1.4876) as specified in SEW 470. Requirements regarding these grades are based on extensive research, together with regression analyses regarding the influence of the chemical composition on the service life.

Grade X 5 NiCrAlTi 32 20 is intended for service temperatures of 500 to 700 °C. When used at temperatures around 500 °C, and when supplied in the annealed for recrystallization condition, this steel grade offers certain advantages. Grade X 8 NiCrAlTi 32 21 is suitable for service temperatures of 700 to 1000 °C.

Comparison of similar materials as specified in this standard and in ISO 2604-2:1975

DIN 17 459		ISO 2604-2	1)
Material designation	Material number		
X6CrNi 1811	1.4948	TS 48	0
X3 CrNiN 1811	1.4949		
XBCrNiTi 1810	1.4941	TS 54	0
X 6 CrNiMo 17 13	1.4919	TS 63	•
X 3 CrNiMoN 17 13	1.4910	•	<del>                                     </del>
X 8 CrNiNb 1613	1.4961	TS 56	. 0
X 8 CrNiMoNb 1616	1.4981	TS 67	•
X 8 CrNiMoVNb 1613	1.4988		ļ
X 5 NiCrAITi 31 20	1.4958	<del>-</del>	_
X 8 NiCrAlTi 32 21	1.4959	TS 69	0

- The symbols indicate the degree of conformance of the chemical composition of the materials covered here, as compared with ISO 2604-2: 1975, as follows:
  - = slightly different;
  - 0 = substantially different.
- Obtainable from Verlag Stahleisen mbH, Postfach 82 29, D-4000 Düsseldorf 1.
- Obtainable from Maximilian-Verlag, Postfach 23 52, D-4900 Herford.

### International Patent Classification

C 22 C 38/40 F 16 L 9/02 G 01 M 3/00 G 01 N 33/20