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July 1976

**Heat Resisting and Highly Heat Resisting Materials
for Bolts and Nuts
Quality Specifications**

**DIN
17 240**

**Warmfeste und hochwarmfeste Werkstoffe für Schrauben
und Muttern; Gütevorschriften**

Sections marked with a dot (•) show when agreements should be made or can be made at the time of ordering.

1 Scope

1.1 This Standard applies to bars and wire of the materials according to Table 1 of dimensions up to those given in Table 4. These materials are normally used for bolts and nuts according to DIN 267 Part 13 — Bolts, screws, nuts and similar threaded and formed parts; technical conditions of delivery; bolts and nuts primarily of steels exhibiting toughness at subzero temperatures and hightemperature steels — at temperatures above about 300 °C up to the maximum service temperatures quoted in Table 4 as a guide for long-term operation. These temperatures may be exceeded where the properties of the material are adequate for the service stresses. The criterion is the total loading on the material resulting from temperature, mechanical loading and the ambient media during the proposed time of operation.

1.2 For bolts and nuts used at temperatures below 300 °C, steels according to

DIN 1651 Free cutting steels; technical conditions of delivery

DIN 1654 Drawn steel for cold pressed screws (bolts); quality specifications (new edition in course of preparation)

DIN 17 100 Steels for general structural purposes; quality specifications

DIN 17 111 Low-carbon unalloyed steels for bolts, nuts and rivets; quality specifications

DIN 17 200 Quenched and tempered steels; quality specifications

DIN 17 210 Case hardening steels; quality specifications

DIN 17 440 Stainless steels; quality specifications

Stahl-Eisen-Werkstoffblatt (Steel-Iron Data Sheet) 550
Steels for large forgings
should be used.

2 Definitions

2.1 Within the meaning of this Standard, materials are considered to be heat resisting if they have good mechanical properties under longtime loading, including high creep limits and high creep rupture strengths and a satisfactory relaxation resistance (see Section 2.2) at temperatures of up to \approx 540 °C, and, as highly heat resisting, steels and alloys having the same characteristics to \approx 800 °C.

2.2 Relaxation means the reduction in the pre-stress in bolts as a result of creep of the material. In this Standard, the residual stress to which the initial stress δ_A corresponding to an initial strain ϵ_A total falls after a defined period of loading, e.g. 1000, 10 000 or 30 000 hours, is quoted to characterize the relaxation resistance of materials (see Table 10).

2.3 For technical definitions and expressions relating to heat-treatment of ferrous metals, see DIN 17 014 Part 1.

3 Dimensions and permissible dimensional deviations

3.1 The dimension standards listed at the end of this Standard apply to products made from materials according to this Standard, however in the case of materials X 22 CrMoV 12 1 to NiCr20TiAl (see Table 1) not all the dimensions listed in the dimension standards quoted can be supplied and not all the permitted deviations can be maintained. Where applicable, the manufacturer should draw attention to this fact when accepting an order.

3.2 • If no dimensional standards exist for products, the permissible dimensional deviations should, if necessary, be agreed at the time of ordering.

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4 Calculation of weight and permissible weight deviations

4.1 Calculation of the nominal weight of products should be based on the densities quoted in Table 7.

4.2 • If the permissible weight deviations have not been standardized, they should if necessary be agreed at the time of ordering.

5 Classification by grades

5.1 Materials

This Standard covers the steels and alloys quoted in Table 1.

5.1.1 The choice of grade of material is left to the customer. It is recommended that the manufacturer be brought in for consultation.

5.2 As-delivered condition

5.2.1 • The treatment condition in which the material is to be supplied shall in all cases be specified by the customer. Table 3 lists the treatment conditions in which materials can normally be supplied. These are not in all cases identical with the normal heat-treatment conditions for the finished bolts and nuts (see Table 4).

5.2.2 The materials from different melts shall be delivered separately and similarly, where applicable, batches of material having received different heat treatment and material of different dimension ranges.

6 Designation

6.1 The code numbers for the steels are formed in accordance with Section 2.1.2.2 of the explanations in Normenheft 3 (1970 issue), the material numbers for the steels according to DIN 17 007 Part 2 and the material number for the alloy NiCr20TiAl according to DIN 17 007 Part 4. The code letter or suffix number for the treatment condition according to Table 3 should be appended as appropriate to the code number or material number respectively.

Example for steel 24 CrMo 5, material number 1.7258, in quenched and tempered condition (V or .05) : 24 CrMo 5 V or 1.7258.05.

Treatment conditions for which no code letters or suffix numbers have not yet been stipulated at the present time, should be quoted in the order by writing out in full¹⁾.

6.2 The code number or material number for the grade of material and the code letter or suffix number for the treatment condition shall be appended to the symbol for the product as given in the examples of designation in the dimension standards.

Example:

Designation of a hot-rolled round steel of 65 mm diameter of steel grade 24 CrMo 5 in the quenched and tempered condition (see example in Section 6.1):

Round 65 DIN 1013 — 24 CrMo 5 V
or Round 65 DIN 1013 — 1.7258.05

7 Requirements

7.1 • Melting process

It is left to the manufacturer to decide on the melting process, unless this has been agreed at the time of ordering. It must however be notified to the customer if required.

7.2 Chemical composition

7.2.1 The chemical composition determined in the ladle analysis shall conform to Table 1.

7.2.2 The customer can accept slight deviations from the composition limits provided these have no more than an insignificant effect on the properties of the material in use.

7.2.3 • The chemical composition of the melt shall be notified to the customer on request.

7.2.4 • Proof that the product analysis meets the limiting values for the ladle analysis given in Table 1, within the permissible deviations quoted in Table 2, can be agreed at the time of ordering.

7.3 Mechanical properties

7.3.1 The values for mechanical properties at room temperature or at elevated temperature, listed in Tables 4 and 5, are guaranteed for longitudinal specimens (see Fig. 1) of bars and wires supplied in the heat-treatment condition listed in Tables 4 and 5 (see also Fig. 2). In cases where the as-delivered condition (see Table 3) does not correspond to the heat-treatment condition given in Table 4 or 5, the values in these Tables apply to longitudinal specimens taken from the specimen sections after heat-treatment of the latter in accordance with the data in Table 4 or 5 and Table 8.

• Note : If for example, in order to save material, transverse specimens are used for testing, in general the values given in Table 4 or 5 for the yield point and tensile strength can be used as a basis for acceptance. In this case, the values to be maintained for elongation, reduction in area and absorbed energy should be specially agreed (note also Section 8.3.2). In cases of doubt however, for the yield point and tensile strength also, acceptance should be based on the values determined on longitudinal specimens.

7.3.2 Guide information for the long-time strength properties at elevated temperatures and the stress relaxation properties of the materials are given in Table 9 and 10 or in Figs 4 to 7. The values stated are mean values of the scatter bands so far observed and, in the case of the long-time strength properties at elevated temperature, mean values for smooth and notched specimens. It can be assumed that the lower limit of the scatter band for the creep strength of smooth and notched specimens is about 20 % lower than the values stated. The values will be checked again from time to time as further test results become available and, where necessary, corrected.

7.3.3 Guide values for the static modulus of elasticity of the materials as a function of temperature are given in Table 6 and Fig. 3.

¹⁾ See also DIN 17-007 Part 4 (July 1963 issue)
— Material numbers, principal groups 2 and 3, non-ferrous metals —. See especially Section 4 — Appended numbers — and Table 3.

7.4 Physical properties

7.4.1 Guide information for density, thermal expansion, thermal conductivity and specific heat of materials are given in Table 7.

7.5 • Chemical properties

As regards the effect of chemically active substances (corrosion) on the steels referred to in this Standard and in particular the influence of temperature on the chemical behaviour, it is only possible to give useful information for each case separately. It is therefore advisable where necessary to discuss this with the manufacturer describing the particular operating conditions as precisely as possible.

7.6 Surface condition

7.6.1 The products shall have a smooth surface as far as consistent with the shaping process used.

7.6.1.1 In the case of products intended for machining, surface defects, e.g. scabs, grooves, laps, cracks and surface decarburization²⁾ must be contained within the machining allowance; they may be removed by suitable methods provided this does not prejudice the intended application.

7.6.1.2 • In the case of products intended for shaping without cutting (e.g. drop forging or rod drawing), where special requirements exist as to surface condition, this should be expressly stated in the order. In this case, surface defects that would split open during forming must be smoothed out by suitable means. The minimum permissible thickness according to the dimensional standards must however be maintained; it is only permissible to go slightly below this with the agreement of the customer.

7.6.2 Correcting of surface defects by welding is not permitted.

8 Testing

8.1 • Delivery testings

For all materials in this Standard, the customer can agree delivery testings, which in general will be carried out by experts from the manufacturing works or, by special agreement at the time of ordering, also by other inspectors appointed by the customer. When wire is supplied in coils however, no delivery testings are normally carried out.

8.2 Extent of testing

8.2.1 • Materials are classified for testing by melt, with heat treated material separate and by dimension ranges (see Section 8.2.1.1) so as to obtain one or more test units as required. Where no details are stated in Sections 8.2.2 to 8.2.6, the extent of testing (i.e. the number of specimens to be taken per test unit) shall be agreed at the time of ordering.

8.2.1.1 The diameter or distance across flats of the thickest product in a test unit may be a maximum of 1.5 times the corresponding dimension of the thinnest product.

8.2.2 • If the rechecking of the chemical composition of the product has been agreed at the time of ordering, the extent of testing should be stipulated at the same time.

8.2.3 For a delivery testing, uniform strength of a test unit must be proved by hardness testing or (after agree-

ment with the customer or his agent) by some other equivalent process.

8.2.3.1 The hardness testing shall be carried out

- a) in the case of bars with a diameter of more than 120 mm, on one bar per test unit.
- b) in the case of bars with a diameter of 120 mm or less, on 10% of the bars in a test unit, subject to a minimum of 10 bars or, in the case of test units containing less than 10 bars, on each bar.

If the hardness values thus obtained correspond to the upper or lower limit of the prescribed range for tensile strength, the extent of testing shall be increased to 20%. If hardness values are obtained with the 10% or 20% sample corresponding to the limits of the range for tensile strength, 100% of the bars should be tested. In assessing the measured hardness values, account should be taken of the mean uncertainty of measurement as defined in DIN 50 150.

In the case of non-continuous heat-treatment, the bars intended for hardness measurement shall be distributed uniformly over the test unit. In the case of continuous heat-treatment, a larger number of specimens shall be taken from the first layer of bars in proportion to the rest of the test unit.

8.2.3.2 On the bars being tested, hardness shall be measured at one end of each bar, i.e. on half of them at one end and on the other half at the other end.

8.2.3.3 For the tensile test, one specimen each shall be taken from the hardest and softest bar in each test unit determined as in Section 8.2.3.1.

8.2.4 • If the 0.2 limit has to be rechecked at elevated temperatures, the extent of testing shall be agreed at the time of ordering. In general, the 0.2 limit will be rechecked only on one specimen per melt and only at one temperature above room temperature.

8.2.5 The notch bar impact bending test shall be carried out on the same specimens (and specimen sections) as the tensile specimens have been taken from (see Section 8.2.3).

8.2.6 Alloy materials shall be subjected to a suitable testing to detect any incorrect identification of the material.

8.3 Sampling

8.3.1 For the analysis of the product, chips shall be cut uniformly over the complete cross-section of the product being tested.

8.3.2 • For the tensile test, longitudinal specimens shall be taken from the bars selected as in Section 8.2.3.3, in such a manner that the axis of the specimen in the case of bars with dimensions up to 40 mm shall be coincident with the longitudinal axis of the bar and, with bars of over 40 mm, shall lie one sixth of the bar thickness below the surface or as near as possible to this position (see Fig. 1). If the testing of transverse specimens is agreed (see note to Section 7.3.1) the position of the specimens shall be agreed at the time of ordering.

8.3.3 For determination of the 0.2 limit at elevated temperature, specimens shall be taken as for the tensile test according to Section 8.3.2.

²⁾ In this context, surface decarburization shall be understood as the sum of the width of the decarbonized zone and 2/3 the width of the carbide-reduced zone.

8.3.4 The specimens for the notch bar impact bending test shall be taken in such a manner that their longitudinal axis lies in the product approximately in the same way as that of the tensile specimens according to Section 8.3.2 (Note Section 8.5.4.1).

8.3.5 The specimens to be taken for the tests and the bars from which the specimens are taken shall be adequately marked so that specimen and bar are clearly identified as belonging together.

8.4 Marking

Each bar exceeding 25 mm in diameter or across flats shall be marked at one end with the melt number, the manufacturer's symbol and the code number or material number of the material. In the case of bars of up to 25 mm diameter or across flats, it is sufficient to identify each bundle with a tie-on tag bearing the same information. The same applies to coils of wire of any dimensions.

8.5 Test methods to be used

8.5.1 • The chemical composition shall be tested by the methods³⁾ specified by the Chemists' Committee of the Verein Deutscher Eisenhüttenleute (Association of German Ferrous Metallurgists). Methods not specified by the Chemists' Committee shall be specially agreed.

8.5.2 The tensile test shall be carried out according to DIN 50 145, using the short proportional bar with gauge length $L_0 = 5 d_0$ according to DIN 50 125. The 0.2 limit shall be determined at room temperature according to DIN 50 145.

8.5.3 The 0.2 limit at elevated temperature shall be determined, where required, according to DIN 50 145.

8.5.4 The notch bar impact bending test shall be carried out on the basis of the information in Table 4 on ISO V-notch specimens or on DVM specimens according to DIN 50 115.

8.5.4.1 • In general, the absorbed energy shall be determined as the mean of three tests on specimens lying side by side at the same distance from the surface or, if this is impossible, immediately behind each other in the same specimen bar; proof of the absorbed energy on only one or two specimens may however be agreed at the time of ordering. In arbitration cases, the mean of three specimens shall be taken.

8.5.4.2 • For products of dimensions such that it is not possible to take a notch impact specimen of standardized dimensions, special agreements shall be made at the time of ordering for carrying out the notch bar impact bending test.

8.5.5 The Brinell hardness shall be determined according to DIN 50 351.

8.5.6 • As regards the method for rechecking the surface decarburization, where required, agreement should be made at the time of ordering.

8.5.7 A test standard for determining the relaxation properties is being prepared.

8.6 Repeat testings

8.6.1 Where an unsatisfactory result in a testing is clearly due to inadequacies in the testing technique or an insignificant local defect in a specimen, the unsatisfactory result should be ignored when deciding whether the requirements have been met and the test concerned repeated.

8.6.2 If the unsatisfactory result of a testing can be traced to unsatisfactory heat-treatment, the bars of the corresponding test unit may be heat-treated again and the whole testing should then be repeated.

8.6.3 If the result of a tensile test on properly heat-treated material does not meet the prescribed requirements, proceed as follows.

If there are other bars of the same hardness among those tested in the same test unit, further specimens for the tensile test and the notch bar impact bending test shall be taken from two of these bars. If there are no further bars of the same hardness among those tested in the same test unit, the extent of hardness testing should be doubled. According to the result of the first (unsatisfactory) tensile test, the repeat testings shall be carried out on specimens from the two softest or two hardest bars of all those checked.

If the result of the notch bar impact bending test on properly heat-treated material does not meet the prescribed requirements, further specimens shall be taken from any two other bars of the test unit without increasing the extent of hardness testing.

8.6.3.1 Properly heat-treated bars having unsatisfactory test results shall in all cases be rejected. Both repeat testings must meet the prescribed requirements, otherwise the complete test unit may be rejected. If necessary, the bars can then be tested separately and certified as meeting the conditions if the results are satisfactory.

8.7 Test certificates

The delivery testing is certified by one of the certificates according to DIN 50 049. The type of certificate must be agreed at the time of ordering.

9 Hot forming and heat-treatment

Table 8 gives information on the temperatures (and hold times) to be used for hot forming and heat-treatment.

10 Complaints⁴⁾

10.1 Objections may only be raised to external or internal defects if they impair to an appreciable extent appropriate working and utilization of the grade of steel and shape of product.

10.2 The customer must give the supplier the opportunity to check for himself the validity of the objection, where possible by submitting the material complained of together with samples of the material supplied.

³⁾ Handbuch für das Eisenhüttenlaboratorium (Handbook for the Ferrous Metallurgical Laboratory), Vol. 2: Investigation of Metallic Materials; Vol. 4: Arbitration Analyses, Düsseldorf, Verlag Stahleisen mbH, using the latest edition.

⁴⁾ For explanations on this objections clause in quality standards for iron and steel, see DIN-Mitt. (DIN News) Vol. 40 (1961) No. 2, pp. 111/12.

The following dimension standards apply for the materials in this Standard

For hot rolled wire

DIN 59 110 Steel wire rod; dimensions, permissible variations, weights

DIN 59 115 Steel wire rod for bolts, nuts and rivets; dimensions, permissible variations, weights

For hot rolled and hot forged rods

DIN 1013 Steel bars, hot rolled round steel; dimensions, weights, permissible variations

DIN 59 130 Hot rolled round steel bars for bolts and rivets; dimensions, weights, permissible deviations

DIN 1015 Steel bars, hot rolled hexagon steel; dimensions, weights, permissible variations

DIN 7527 Part 6 Steel forgings; machining allowances and permissible variations for open-die forged bars

For bright rods and wires

DIN 668 Bright round steel; dimensions, permissible variations according to ISA tolerance zone h11, weights

DIN 670 Bright round steel; dimensions, permissible variations according to ISA tolerance zone h8, weights

DIN 671 Bright round steel; dimensions, permissible variations according to ISA tolerance zone h9, weights

DIN 176 Bright drawn hexagon steel; dimensions, permissible variations, weights

Table 1. Chemical composition of heat resisting and highly heat resisting materials for bolts and nuts (ladle analysis)

| Material Code number | Material number | C | Si | Mn | P maximum | S | Chemical composition in % by wt. | | | | | | |
|----------------------------|-----------------|--------------------|----------------------------------|--------------------|--------------|-------|----------------------------------|----------------------|--------------------|--------------------|--------------------|----------------------|------------------------------|
| | | | | | | | Al | B | Cr | Mo | Ni | Ti | V |
| C 35 ¹⁾ | 1.0501 | 0,32 to 0,39 | 0,15 to 0,35 | 0,50 to 0,80 | 0,045 | 0,045 | | | | | | | |
| Cr 35 | 1.1181 | 0,32 to 0,39 | 0,15 to 0,35 | 0,50 to 0,80 | 0,035 | 0,035 | | | | | | | |
| Cq 35 | 1.1172 | 0,32 to 0,39 | 0,15 to 0,40 ⁴⁾ | 0,50 to 0,80 | 0,035 | 0,035 | | | | | | | |
| 24 CrMo 5 | 1.7258 | 0,20 to 0,28 | 0,15 to 0,35 | 0,50 to 0,80 | 0,030 | 0,035 | | | | | | | |
| 21 CrMoV 5 7 ²⁾ | 1.7709 | 0,17 to 0,25 | 0,15 to 0,35 | 0,35 to 0,85 | 0,030 | 0,035 | | | | | | | |
| 40 CrMoV 4 7 | 1.7711 | 0,36 to 0,44 | 0,15 to 0,35 | 0,35 to 0,85 | 0,030 | 0,035 | | | | | | | |
| X 22 CrMoV 12 1 | 1.4923 | 0,18 to 0,24 | 0,10 to 0,50 | 0,30 to 0,80 | 0,035 | 0,035 | | | | | | | |
| X 19 CrNiMoNbN 11 1 | 1.4913 | 0,16 to 0,22 | 0,10 to 0,50 | 0,30 to 0,80 | 0,035 | 0,035 | | | | | | | |
| X 8 CrNiMoBNb 16 16 | 1.4986 | 0,04 to 0,10 | 0,30 to 0,60 | ≤1,5 to 0,60 | 0,045 | 0,030 | ≤0,010 | 10,0 to 0,10 | 0,50 to 1,00 | 0,30 to 1,00 | 0,10 to 0,80 | 0,25 to 0,80 | 0,35 |
| NiCr20TiAl ³⁾ | 2.4952 | ≤0,10 | ≤1,00 | ≤1,00 | 0,030 | 0,015 | 1,00 | ≤0,008 to 1,80 | 18,0 to 21,0 | ≥65 | 1,8 to 2,7 | Co ≤2,00 Fe ≤3,00 | Nb + Ta: 10 x % C to 1,20 |

¹⁾ Only usable for nuts.²⁾ Instead of bolts and nuts of this steel, it is possible for a transitional period to use also bolts and nuts of steels 24 CrMoV 5 5 (material number 1.7733) and 21 CrMoV 5 11 (material number 1.8070) (see Explanations). In special cases, it is possible also to use steel 21 CrMoNiV 4 7 (material number 1.6981) instead of this material.³⁾ For this alloy, in all cases the values given in the latest issue of DIN 17 742 apply.
⁴⁾ • Lower silicon contents may be agreed at the time of ordering, in which case any resulting changes in the guaranteed properties must be taken into account.

Table 2. Permissible deviation of the bar analysis from the limiting values for the ladle analysis for the steels in Table 1¹⁾

| Element | Permissible maximum contents in the ladle analysis % by wt. | Permissible deviations of bar analysis from the limiting values of the ladle analysis 2), 3) % by wt. |
|-----------|---|---|
| C | < 0,20 ≥ 0,20 ≤ 0,44 | ± 0,01 ± 0,02 |
| Si | ≤ 1,0 | ± 0,05 |
| Mn | ≤ 1,5 | ± 0,04 |
| P | ≤ 0,045 | ± 0,005 |
| S | ≤ 0,045 | ± 0,005 |
| N | ≤ 0,10 | ± 0,01 |
| Cr | ≤ 2,00 > 10 ≤ 15,0 > 15 ≤ 20,0 | ± 0,05 ± 0,15 ± 0,20 |
| Mo | ≤ 0,35 > 0,35 ≤ 2,00 | ± 0,04 ± 0,05 |
| Ni | ≤ 1,00 ≥ 15,5 ≤ 17,5 | ± 0,03 ± 0,15 |
| Nb (+ Ta) | ≤ 1,20 | ± 0,05 |
| V | ≤ 0,35 | ± 0,03 |

1) • For the alloy NiCr20TiAl, and for the boron contents of steels, where necessary the permissible deviations should be agreed at the time of ordering.
 2) • Applies to diameters ≤ 160 mm or cross-sections of equivalent area. For forgings, the permissible deviations should be agreed at the time of ordering.
 3) It is permissible for the deviation for an element in the bar analysis for a melt to be entirely below the minimum value or entirely above the maximum value of the range given for the ladle analysis but not both at the same time.

Table 3. Normal as-delivered conditions and associated code letters and suffix numbers in the material numbers

| Material | | Normal as-delivered conditions (X) | | | | | | | |
|---|-----------------|------------------------------------|------------|---------------|--------------|--------------------------|----------------------|---------------------------|--|
| Code number | Material number | untreated (= hot formed) | normalized | soft annealed | spheroidized | quenched and tempered | solution annealed | precipitation hardened | hot strain hardened + age hardened |
| C 35 | 1.0501 | X | X | | | X | | | |
| Ck 35 | 1.1181 | X | X | | | X | | | |
| Cq 35 | 1.1172 | X ¹⁾ | | | X | | | | |
| 24 CrMo 5 | 1.7258 | X | | X | | X | | | |
| 21 CrMoV 5 7 | 1.7709 | X | | X | | X | | | |
| 40 CrMoV 4 7 | 1.7711 | | | X | | X | | | |
| X 22 CrMoV 12 1 | 1.4923 | | | X | | X | | | |
| X 19 CrMoVNbN 11 1 | 1.4913 | | | X | | X | | | |
| X 8 CrNiMoBNb 16 16 | 1.4986 | | | | | | | | X |
| NiCr20TiAl | 2.4952 | X | | | | | X | X | |
| Code letter ^{2), 3)} | | U | N | G | (GKZ) | V | (L) | (AH) | (WK + AL) |
| Suffix numbers in the material number ²⁾ | | 00 | 01 | 02 | 4) | 05 | 4) | 4) | 4) |

1) This as-delivered condition is normal only for deliveries to works having their own annealing facilities.
 2) For the as-delivered condition quoted above.
 3) The code letters in brackets have not so far been standardized. They are used here merely as an aid for abbreviated designation of the as-delivered conditions in the Tables.
 4) Not yet stipulated in DIN 17007 Part 2.

Table 4. Guaranteed values for mechanical properties at room temperature of heat resisting and highly heat resisting materials for bolts and nuts (applies to longitudinal specimens)

| Code number | Material number | Condition 2) V | Applicable for diameters mm | Yield point or 0.2 % proof stress N/mm ² min. | Mechanical properties at room temperature | | | Guidance value for normal upper limit of temperature of use in con- tinuous operation |
|---------------------|-----------------|-------------------|--------------------------------------|--|---|---|---------------------------|--|
| | | | | | Tensile strength N/mm ² | Elong- ation ($L_0 = 5 d_0$) % | Reduction in area % | |
| C 35 1) | 1.0501 | N | ≤ 100 | 280 | 500 to 650 | 21 | — | — |
| Ck 35 | 1.1181 | V | ≤ 60 | 280 | 500 to 650 | 22 | 40 | — |
| Cq 35 | 1.1172 | V ⁵⁾ | $> 60 \leq 160$ | 280 | 500 to 650 | 22 | 45 | 55 39 |
| 24 CrMo 5 | 1.7258 | V | $> 100 \leq 160$ | 440 | 600 to 750 | 18 | 60 | 55 39 |
| 21 CrMoV 5 7 | 1.7709 | V | ≤ 250 | 280 | 500 to 650 | 22 | 45 | 55 39 |
| 40 CrMoV 4 7 | 1.7711 | V | ≤ 100 | 420 | 600 to 750 | 18 | 60 | 103 89 |
| X 22 CrMoV 12 1 | 1.4923 | V | ≤ 250 | 550 | 700 to 850 (6) | 16 | 60 | 118 102 |
| X 19 CrMoVNbN 11 1 | 1.4913 | V | ≤ 250 | 700 | 850 to 1000 (6) | 14 | 45 | 55 40 |
| X 8 CrNiMoBNb 16 16 | 1.4986 | (WK + AL) | ≤ 100 | 600 | 800 to 950 | 14 | 40 | 400 40 |
| NiCr20TiAl | 2.4952 | (AH) | ≤ 160 | 600 | 650 to 850 | 16 | 40 | 34 27 |
| | | | | | ≥ 1000 | 12 | 12 | 580 580 |
| | | | | | | 17 | 17 | 580 580 |
| | | | | | | | 20 | 580 580 |
| | | | | | | | | 650 650 |
| | | | | | | | | 700 700 |

1) Only usable for nuts.

2) See also Tables 3 and 8.

3) For acceptance testing, agreement can be made as to which of the two shapes of specimen quoted is to be used. If the values obtained for absorbed energy are below the minimum required values for ISO V-notch specimens, proceed as if the proof of absorbed energy were required on DVM specimens.

4) In the case of nuts, the normal upper limit of temperature of use in continuous operation can be 50 °C higher.

5) Because of its subsequent working by cold-forming, steel Cq 35 is normally supplied in the "spheroidized" (GKZ) condition.

6) The upper limit of the tensile strength range must not be exceeded; values slightly below the lower limit of the tensile strength range are permissible provided the minimum value for the yield point is reached.

7) The values given are provisional values that will have to be checked.

Table 5. Guaranteed values for yield point at elevated temperatures of heat resisting and highly heat resisting materials for bolts and nuts (applicable to longitudinal specimens)

| Code number | Material number | Condition ¹⁾ | Applicable for diameters mm | Yield point or 0.2 % stress limit at a temperature of ²⁾ , ³⁾ | | | | | | | |
|---------------------|-----------------|-------------------------|-----------------------------|---|--------|--------|--------|--------|--------|--------|--------|
| | | | | 20 °C | 200 °C | 250 °C | 300 °C | 350 °C | 400 °C | 450 °C | 500 °C |
| N/mm ² | | | | | | | | | | | |
| Ck 35 | 1.1181 | V | ≤ 160 | 280 | 220 | 203 | 186 | 167 | 147 | — | — |
| Cq 35 | 1.1172 | V | ≤ 40 | 280 | 220 | 203 | 186 | 167 | 147 | — | — |
| 24 CrMo 5 | 1.7258 | V | ≤ 100 | 440 | 412 | 392 | 363 | 333 | 304 | 275 | 235 |
| | | | > 100 ≤ 160 | 420 | 382 | 372 | 344 | 324 | 294 | 265 | 226 |
| 21 CrMoV 5 7 | 1.7709 | V | ≤ 250 | 550 | 500 | 480 | 460 | 441 | 412 | 372 | 334 |
| 40 CrMoV 4 7 | 1.7711 | V | ≤ 100 | 700 | 635 | 617 | 598 | 578 | 540 | 500 | 460 |
| X 22 CrMoV 12 1 | 1.4923 | V | ≤ 250 | 600 | 530 | 505 | 480 | 452 | 423 | 382 | 344 |
| X 19 CrMoVNBN 11 1 | 1.4913 | V | ≤ 250 | 700 | 603 | 578 | 550 | 515 | 485 | 442 | 392 |
| X 8 CrNiMoBNb 16 16 | 1.4986 | (WK + AL) | ≤ 100 | 500 | 432 | 412 | 393 | 372 | 353 | 530 | 470 |
| NiCr20TiAl | 2.4952 | (AH) | ≤ 160 | 600 | 568 | 564 | 560 | 550 | 540 | 530 | 520 |
| | | | | | | | | | | 510 | 500 |
| | | | | | | | | | | 480 | |

¹⁾ See Tables 3 and 8.

²⁾ For unalloyed and low alloy ferritic-pearlitic steels, the yield point, or when there is no clearly defined yield point, the 0.2% limit is the criterion but for other materials only the 0.2% limit.

³⁾ The values for temperatures lying above the point of intersection with the corresponding creep limit curve, are guide values and are not subject to checking.

Table 6. Guidance values for the static modulus of elasticity of heat resisting and highly heat resisting materials for bolts and nuts

| Material group 1) | | Static modulus of elasticity at a temperature of 10 ³ N/mm ² | | | | | | | | | | |
|---|--|---|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| | | 20 °C | 100 °C | 200 °C | 300 °C | 400 °C | 450 °C | 500 °C | 550 °C | 600 °C | 700 °C | 800 °C |
| Ferritic steels (1.0501, 1.1181, 1.1172, 1.7258, 1.7709, 1.7711) | | 211 | 204 | 196 | 186 | 177 | 172 | 164 | 152 | 127 | — | — |
| Steels with about 12% Cr (1.4923, 1.4913) | | 216 | 209 | 200 | 190 | 179 | 175 | 167 | 157 | 127 | — | — |
| Austenitic steels (1.4986) | | 196 | 192 | 186 | 181 | 174 | 170 | 165 | 161 | 157 | 147 | — |
| NiCr20TiAl | | 216 | 212 | 208 | 202 | 196 | 193 | 189 | 184 | 179 | 161 | 130 |

¹⁾ Steels belonging to the material groups listed are quoted by their material number.

Table 7. Guidance values for the physical properties of heat resisting and highly heat resisting materials for bolts and nuts

| Material Code number | Material number | Density at 20 °C kg/dm ³ | Coefficient of thermal expansion between 20 °C and 100 °C | | | | | | (Mean) thermal conductivity ¹⁾ at °C W K · m | (Mean) specific heat capacity ¹⁾ at °C J kg · K | |
|-------------------------|--------------------|---|--|--------|--------|--------|--------|--------|---|--|----------------------|
| | | | 100 °C | 200 °C | 300 °C | 400 °C | 500 °C | 600 °C | | | |
| C 35 | 1.0501 | 7,85 | 11,1 | 12,1 | 12,9 | 13,5 | 13,9 | 14,1 | 20 | 42 | 20 |
| Ck 35 | 1.1181 | | | | | | | | 20 | 33 | 20 |
| Cq 35 | 1.1172 | | | | | | | | 20 | 33 | 20 |
| 24 CrMo 5 | 1.7258 | | | | | | | | 20 | 42 | 20 |
| 21 CrMoV 5 7 | 1.7709 | | | | | | | | 20 | 33 | 20 |
| 40 CrMoV 4 7 | 1.7711 | | | | | | | | 20 | 33 | 20 |
| X 22 CrMoV 12 1 | 1.4923 | 7,7 | 10,5 | 11 | 11,5 | 12 | 12,3 | 12,5 | 20 to 650 | 24 29 | 20 0 to 800 |
| X 19 CrMoVNbN 11 1 | 1.4913 | | | | | | | | 20 to 650 | 24 29 | 20 0 to 800 |
| X 8 CrNiMoBNb 16 16 | 1.4986 | 7,9 | 16,6 | 17,7 | 17,9 | 17,9 | 18,1 | 18,3 | 18,6 650 | 15 25 | 20 0 to 800 |
| NiCr20TiAl | 2.4952 | 8,2 | 11,9 | 12,6 | 13,1 | 13,5 | 13,7 | 14,0 | 14,5 100 900 | 13 12 28 | 20 20 0 to 800 |

¹⁾ In most cases these are the results of measurements on individual melts. When further test results become available, it is intended to standardize values and where necessary correct them.

Table 8. Information for hot forming and heat treatment of heat resisting and highly heat resisting materials for bolts and nuts¹⁾

| Material Code number | Material number | Hot forming °C | Hardening, quenching or solution annealing °C | Cooling in | Tempering or age hardening or precipitation hardening °C | Stress-relief annealing °C |
|----------------------------|--------------------|---------------------------|--|---------------|---|----------------------------------|
| C 35 | 1.0501 | 1100 to 850 | 870 to 900 | Oil | 650 to 710, min. 2 h | 550 to 620 |
| Ck 35 | 1.1181 | | | | | |
| Cq 35 | 1.1172 | | | | | |
| 24 CrMo 5 | 1.7258 | 1100 to 850 | 900 to 950 | Oil or air | 650 to 710, min. 2 h | 550 to 620 |
| 21 CrMoV 5 7 ²⁾ | 1.7709 | 1100 to 850 | 890 to 940 | Oil or air | 680 to 720, min. 2 h | 580 to 650 |
| 40 CrMoV 4 7 ²⁾ | 1.7711 | 1100 to 850 | 880 to 930 | Oil (or air) | 670 to 730, min. 2 h | 570 to 640 |
| X 22 CrMoV 12 1 | 1.4923 | 1100 to 850 | 1020 to 1070 | Air or oil | 640 to 720, min. 2 h | 600 to 680 |
| X 19 CrMoVNBN 11 1 | 1.4913 | 1100 to 850 | 1100 to 1150 | Air or oil | 670 to 750, min. 2 h | 630 to 710 |
| X 8 CrNiMoNbN 16 16 | 1.4986 | 1150 to 850 ³⁾ | — | — | 750 to 800, 5 to 1 h/air | 750 to 800 |
| NiCr20TiAl ⁴⁾ | 2.4952 | 1150 to 1050 | 1050 to 1080, 8 h | Air | 840 to 860, 24 h/air and 690 to 710, 16 h/air | — |

- 1) The temperatures for hot forming are guide values, the other information should as far as possible be complied with.
 2) Because of its importance with regard to embrittlement, it is not permissible to go above the quenching temperature or below the tempering temperature quoted.
 3) Hot strain hardening at 750 to 850 °C.
 4) The complete, three-stage heat-treatment should be carried out after the last plastic forming operation (e.g. after thread rolling).

Table 9. Guidance values for the long-time high temperature strength values

| Material Code number | Material number | Temper- ture °C | 0.2 % creep limit for a time of 10000h 30000h 100000h N/mm ² | | | 1 % creep limit for a time of 10000h 30000h 100000h N/mm ² | | | Creep rupture strength for 10000h 30000h 100000h N/mm ² | | |
|---|--------------------|-----------------------|--|--------|---------|--|--------|---------|---|--------|---------|
| | | | 10000h 30000h 100000h N/mm ² | | | 10000h 30000h 100000h N/mm ² | | | 10000h 30000h 100000h N/mm ² | | |
| | | | 10000h | 30000h | 100000h | 10000h | 30000h | 100000h | 10000h | 30000h | 100000h |
| Ck 35 and Cq 35 | 1.1181 1.1172 | 360 | 199 | 172 | 133 | 208 | 185 | 151 | 246 | 230 | 218 |
| | | 360 | 182 | 157 | 122 | 197 | 177 | 139 | 236 | 215 | 202 |
| | | 370 | 187 | 142 | 112 | 185 | 163 | 130 | 224 | 200 | 186 |
| | | 380 | 149 | 128 | 100 | 174 | 154 | 120 | 212 | 188 | 169 |
| | | 390 | 133 | 114 | 90 | 161 | 140 | 109 | 200 | 174 | 154 |
| | | 400 | 118 | 101 | 79 | 147 | 127 | 98 | 187 | 159 | 138 |
| | | 410 | 103 | 88 | 69 | 132 | 115 | 87 | 173 | 145 | 122 |
| | | 420 | 90 | 77 | 60 | 116 | 100 | 77 | 156 | 130 | 106 |
| | | 430 | 79 | 67 | 51 | 102 | 88 | 67 | 138 | 113 | 93 |
| | | 440 | 68 | 57 | 43 | 89 | 76 | 58 | 118 | 98 | 80 |
| | | 450 | 59 | 49 | 35 | 78 | 66 | 49 | 100 | 86 | 69 |
| | | 460 | 50 | 40 | 29 | 68 | 56 | 40 | 87 | 75 | 61 |
| | | 470 | 43 | 34 | 25 | 58 | 48 | 34 | 77 | 64 | 53 |
| | | 480 | 35 | 29 | 21 | 49 | 41 | 29 | 69 | 55 | 45 |
| | | 490 | 29 | 24 | 18 | 42 | 35 | 26 | 61 | 48 | 39 |
| | | 500 | 25 | 21 | 16 | 35 | 30 | 22 | 53 | 43 | 34 |
| 24 CrMo 5 | 1.7258 | 420 | 204 | 180 | 165 | 274 | 248 | 221 | 387 | 344 | 308 |
| | | 430 | 188 | 170 | 152 | 258 | 230 | 203 | 364 | 322 | 281 |
| | | 440 | 174 | 155 | 138 | 242 | 212 | 186 | 338 | 292 | 253 |
| | | 450 | 162 | 143 | 125 | 226 | 195 | 171 | 311 | 266 | 226 |
| | | 460 | 149 | 130 | 113 | 210 | 180 | 155 | 283 | 240 | 200 |
| | | 470 | 135 | 118 | 100 | 195 | 163 | 141 | 255 | 213 | 178 |
| | | 480 | 124 | 105 | 87 | 180 | 148 | 127 | 226 | 188 | 157 |
| | | 490 | 112 | 94 | 75 | 163 | 135 | 112 | 200 | 165 | 136 |
| | | 500 | 100 | 82 | 64 | 147 | 120 | 98 | 176 | 145 | 118 |
| | | 510 | 88 | 70 | 53 | 130 | 105 | 83 | 153 | 125 | 100 |
| | | 520 | 77 | 58 | 42 | 115 | 90 | 69 | 133 | 106 | 82 |
| | | 530 | 66 | 47 | 32 | 98 | 74 | 54 | 114 | 88 | 66 |
| | | 540 | 55 | 37 | 24 | 81 | 58 | 39 | 95 | 71 | 51 |
| | | 550 | 46 | 29 | 18 | 64 | 41 | 25 | 79 | 54 | 36 |
| 21 CrMo V 7 and 40 CrMo V 47 | 1.7709 1.7711 | 420 | 394 | 373 | 351 | 437 | 409 | 364 | 481 | 445 | 410 |
| | | 430 | 369 | 349 | 323 | 412 | 382 | 338 | 455 | 419 | 385 |
| | | 440 | 343 | 322 | 293 | 387 | 359 | 314 | 429 | 392 | 358 |
| | | 450 | 317 | 294 | 262 | 361 | 334 | 288 | 405 | 364 | 328 |
| | | 460 | 287 | 264 | 228 | 337 | 308 | 265 | 378 | 336 | 299 |
| | | 470 | 267 | 235 | 197 | 313 | 284 | 242 | 351 | 308 | 268 |
| | | 480 | 242 | 204 | 168 | 288 | 259 | 220 | 324 | 281 | 240 |
| | | 490 | 216 | 178 | 142 | 266 | 239 | 197 | 298 | 256 | 207 |
| | | 500 | 191 | 154 | 119 | 242 | 215 | 175 | 271 | 230 | 188 |
| | | 510 | 166 | 131 | 99 | 221 | 193 | 154 | 248 | 208 | 167 |
| | | 520 | 144 | 112 | 83 | 199 | 172 | 132 | 226 | 187 | 146 |
| | | 530 | 123 | 94 | 67 | 177 | 150 | 112 | 207 | 168 | 128 |
| | | 540 | 106 | 81 | 55 | 157 | 130 | 94 | 189 | 151 | 111 |
| | | 550 | 89 | 67 | 44 | 138 | 108 | 74 | 170 | 135 | 95 |
| X 22 CrMo V 12 1, quenched and tempered to 800 to 950 N/mm ² tensile strength | 1.4923 | 450 | 343 | 310 | 264 | 436 | 401 | 373 | 480 | 453 | 432 |
| | | 460 | 314 | 283 | 240 | 405 | 372 | 341 | 451 | 422 | 397 |
| | | 470 | 285 | 256 | 215 | 375 | 338 | 308 | 422 | 396 | 368 |
| | | 480 | 258 | 230 | 193 | 344 | 306 | 278 | 394 | 360 | 336 |
| | | 490 | 230 | 204 | 168 | 316 | 278 | 248 | 366 | 335 | 306 |
| | | 500 | 204 | 179 | 147 | 289 | 254 | 221 | 338 | 304 | 275 |
| | | 510 | 178 | 156 | 127 | 262 | 228 | 195 | 312 | 278 | 245 |
| | | 520 | 155 | 133 | 108 | 235 | 200 | 170 | 286 | 250 | 216 |
| | | 530 | 132 | 114 | 91 | 211 | 177 | 148 | 261 | 222 | 187 |
| | | 540 | 114 | 96 | 77 | 187 | 156 | 127 | 235 | 196 | 161 |
| | | 550 | 96 | 81 | 63 | 165 | 135 | 108 | 211 | 172 | 137 |
| | | 560 | 80 | 67 | 51 | 144 | 117 | 91 | 187 | 150 | 118 |
| | | 570 | 68 | 55 | 41 | 126 | 99 | 77 | 165 | 128 | 99 |
| | | 580 | 58 | 46 | 33 | 108 | 84 | 64 | 143 | 111 | 83 |
| | | 590 | 51 | 39 | 28 | 92 | 71 | 53 | 122 | 93 | 70 |
| X 22 CrMo V 12 1, quenched and tempered to 900 to 1050 N/mm ² tensile strength | 1.4923 | 600 | 46 | 36 | 27 | 79 | 60 | 44 | 103 | 79 | 59 |
| | | 650 | — | — | — | — | — | — | 46 | 35 | 26 |
| | | 700 | — | — | — | — | — | — | 25 | 20 | 14 |
| | | 750 | — | — | — | — | — | — | 14 | — | — |
| | | 800 | — | — | — | — | — | — | 9 | — | — |
| | | 450 | 359 | 322 | 273 | 475 | 450 | 403 | 516 | 489 | 445 |
| | | 460 | 330 | 295 | 249 | 445 | 418 | 372 | 487 | 459 | 414 |
| | | 470 | 300 | 268 | 226 | 415 | 386 | 340 | 458 | 428 | 382 |
| | | 480 | 274 | 242 | 203 | 386 | 356 | 310 | 428 | 398 | 352 |
| | | 490 | 246 | 216 | 180 | 356 | 325 | 280 | 398 | 366 | 319 |
| | | 500 | 219 | 192 | 160 | 327 | 296 | 251 | 368 | 334 | 288 |
| | | 510 | 194 | 168 | 139 | 298 | 266 | 221 | 337 | 303 | 256 |
| | | 520 | 170 | 147 | 119 | 270 | 238 | 193 | 308 | 272 | 226 |
| | | 530 | 148 | 127 | 101 | 242 | 210 | 167 | 278 | 242 | 196 |
| | | 540 | 128 | 108 | 86 | 215 | 183 | 142 | 250 | 215 | 170 |
| | | 550 | 109 | 91 | 70 | 189 | 158 | 120 | 222 | 185 | 144 |
| | | 560 | 92 | 76 | 57 | 166 | 134 | 99 | 196 | 160 | 122 |
| | | 570 | 78 | 62 | 45 | 142 | 114 | 81 | 171 | 136 | 101 |
| | | 580 | 65 | 51 | 37 | 123 | 95 | 65 | 148 | 115 | 84 |
| | | 590 | 55 | 43 | 31 | 104 | 80 | 53 | 126 | 97 | 70 |
| | | 600 | 47 | 37 | 27 | 87 | 66 | 42 | 108 | 82 | 59 |

Table 9. (continued)

| Material Code number | Material number | Temper- ature °C | 0.2 % creep limit for a time of 10000h 30000h 100000h N/mm ² | | | 1 % creep limit for a time of 10000h 30000h 100000h N/mm ² | | | Creep rupture strength for 10000h 30000h 100000h N/mm ² | | |
|---|--------------------|------------------------|--|--------|---------|--|--------|---------|---|--------|---------|
| | | | 10000h | 30000h | 100000h | 10000h | 30000h | 100000h | 10000h | 30000h | 100000h |
| X 19 CrMoVNbN 11 1 | 1.4913 | 450 | 442 | 413 | 373 | 500 | 478 | 448 | 578 | 560 | 530 |
| | | 460 | 408 | 380 | 338 | 475 | 450 | 416 | 545 | 522 | 488 |
| | | 470 | 376 | 348 | 305 | 450 | 423 | 388 | 512 | 485 | 448 |
| | | 480 | 344 | 316 | 274 | 424 | 392 | 358 | 480 | 452 | 410 |
| | | 490 | 315 | 285 | 245 | 398 | 366 | 328 | 450 | 415 | 373 |
| | | 500 | 286 | 257 | 216 | 374 | 339 | 298 | 420 | 382 | 334 |
| | | 510 | 261 | 230 | 191 | 349 | 310 | 268 | 394 | 353 | 298 |
| | | 520 | 238 | 205 | 168 | 323 | 281 | 238 | 368 | 323 | 265 |
| | | 530 | 215 | 181 | 143 | 298 | 253 | 210 | 341 | 292 | 232 |
| | | 540 | 191 | 159 | 120 | 274 | 224 | 181 | 315 | 262 | 201 |
| | | 550 | 170 | 135 | 98 | 250 | 197 | 153 | 289 | 235 | 172 |
| | | 560 | 147 | 113 | — | 225 | 167 | — | 263 | 207 | 144 |
| | | 570 | 127 | 90 | — | 201 | 138 | — | 238 | 180 | 119 |
| | | 580 | 105 | 68 | — | 177 | 110 | — | 213 | 155 | 96 |
| | | 590 | 88 | 45 | — | 154 | 81 | — | 188 | 132 | 75 |
| | | 600 | 69 | 23 | — | 133 | 49 | — | 164 | 111 | 59 |
| X 8 CrNiMoBNb 16 16, hot strain hardened | 1.4986 | 580 | 245 | 200 | 164 | 358 | 328 | 302 | 381 | 352 | 323 |
| | | 590 | 240 | 193 | 158 | 336 | 303 | 278 | 364 | 330 | 298 |
| | | 600 | 235 | 186 | 147 | 324 | 288 | 255 | 344 | 308 | 275 |
| | | 610 | 230 | 180 | 137 | 306 | 264 | 230 | 325 | 288 | 251 |
| | | 620 | 225 | 170 | 126 | 287 | 242 | 204 | 306 | 263 | 228 |
| | | 630 | 210 | 156 | 112 | 268 | 220 | 179 | 287 | 242 | 204 |
| | | 640 | 195 | 145 | 96 | 247 | 196 | 153 | 267 | 220 | 181 |
| | | 650 | 176 | 127 | 79 | 226 | 171 | 128 | 245 | 196 | 157 |
| | | 660 | 145 | 104 | 64 | 204 | 148 | 104 | 221 | 173 | 133 |
| | | 670 | 120 | 85 | 51 | 182 | 125 | 85 | 198 | 151 | 113 |
| NiCr20TiAl | 2.4952 | 500 | 533 | 494 | 452 | 624 | 576 | 530 | (745) | (666) | (578) |
| | | 510 | 516 | 475 | 426 | 608 | 557 | 504 | (711) | (633) | (545) |
| | | 520 | 498 | 452 | 402 | 586 | 533 | 477 | (680) | (601) | (510) |
| | | 530 | 480 | 430 | 377 | 567 | 512 | 450 | 646 | 570 | 480 |
| | | 540 | 462 | 407 | 353 | 544 | 488 | 418 | 615 | 538 | 447 |
| | | 550 | 445 | 386 | 330 | 523 | 465 | 390 | 582 | 510 | 416 |
| | | 560 | 425 | 363 | 309 | 500 | 442 | 362 | 552 | 476 | 384 |
| | | 570 | 410 | 344 | 284 | 474 | 412 | 334 | 520 | 445 | 354 |
| | | 580 | 385 | 321 | 262 | 450 | 386 | 308 | 491 | 417 | 327 |
| | | 590 | 364 | 299 | 243 | 425 | 361 | 282 | 462 | 382 | 298 |
| | | 600 | 343 | 278 | 220 | 398 | 336 | 257 | 433 | 360 | 272 |
| | | 610 | 322 | 259 | 201 | 370 | 311 | 230 | 403 | 333 | 247 |
| | | 620 | 302 | 238 | 181 | 348 | 289 | 210 | 378 | 309 | 222 |
| | | 630 | 283 | 220 | 162 | 326 | 265 | 187 | 351 | 282 | 198 |
| | | 640 | 265 | 202 | 145 | 303 | 245 | 167 | 325 | 258 | 176 |
| | | 650 | 245 | 184 | 128 | 275 | 224 | 149 | 300 | 235 | 157 |
| | | 660 | 228 | 169 | 113 | 260 | 202 | 132 | 275 | 212 | 135 |
| | | 670 | 211 | 152 | 98 | 240 | 185 | 115 | 251 | 190 | 118 |
| | | 680 | 191 | 138 | 84 | 219 | 165 | 99 | 229 | 170 | 102 |
| | | 690 | 174 | 123 | 72 | 201 | 149 | 85 | 208 | 152 | 88 |
| | | 700 | 157 | 110 | 61 | 183 | 133 | 72 | 186 | 133 | 75 |
| | | 710 | 140 | 96 | 52 | 167 | 118 | 64 | 170 | 118 | 65 |
| | | 720 | 125 | 84 | 43 | 150 | 103 | 55 | 153 | 104 | 57 |
| | | 730 | 108 | 71 | 35 | 135 | 90 | 47 | 137 | 93 | 49 |
| | | 740 | 93 | 61 | 30 | 122 | 79 | 40 | 125 | 82 | 44 |
| | | 750 | 83 | 50 | 24 | 106 | 69 | 33 | 114 | 75 | 37 |
| | | 760 | 66 | 41 | 20 | 97 | 59 | 29 | 103 | 67 | 33 |
| | | 770 | 54 | 33 | 16 | 85 | 53 | 24 | 94 | 59 | 29 |
| | | 780 | 45 | 25 | 12 | 75 | 46 | 20 | 86 | 53 | 25 |
| | | 790 | 33 | 20 | 9 | 68 | 40 | 17 | 78 | 47 | 23 |
| | | 800 | 24 | 15 | 5 | 58 | 35 | 16 | 70 | 43 | 20 |

Table 10. Provisional guidance values for the relaxation properties¹⁾

| Material Code number | Material number | Temperature °C | for an initial strain $\epsilon_{A\text{ total}}$ % | Residual stress in N/mm ² after stressing duration for | | |
|-------------------------------------|--------------------|-------------------|---|--|----------|----------|
| | | | | 1000 h | 10 000 h | 30 000 h |
| 21 CrMoV 5 7 and 40 CrMoV 4 7 | 1.7709 | 300 | 0,2 | 328 | 325 | 317 |
| | | 350 | | 314 | 299 | 292 |
| | | 400 | | 288 | 262 | 250 |
| | | 410 | | 281 | 252 | 235 |
| | | 420 | | 273 | 242 | 222 |
| | | 430 | | 263 | 227 | 200 |
| | | 440 | | 253 | 211 | 180 |
| | | 450 | | 239 | 186 | 154 |
| | | 460 | | 224 | 163 | 130 |
| | 1.7711 | 470 | | 208 | 138 | 108 |
| | | 480 | | 191 | 117 | 90 |
| | | 490 | | 172 | 98 | 70 |
| | | 500 | | 150 | 81 | 56 |
| | | 510 | | 128 | 67 | 43 |
| | | 520 | | 109 | 53 | 33 |
| | | 530 | | 92 | 41 | 25 |
| | | 540 | | 75 | 33 | 18 |
| X 22 CrMoV 12 1 | 1.4923 | 400 | 0,2 | 255 | 232 | 216 |
| | | 410 | | 250 | 223 | 206 |
| | | 420 | | 248 | 212 | 193 |
| | | 430 | | 234 | 200 | 180 |
| | | 440 | | 225 | 189 | 170 |
| | | 450 | | 216 | 173 | 155 |
| | | 460 | | 206 | 159 | 140 |
| | | 470 | | 195 | 143 | 125 |
| | | 480 | | 183 | 130 | 110 |
| | | 490 | | 170 | 115 | 98 |
| | | 500 | | 157 | 103 | 85 |
| | | 510 | | 142 | 91 | 75 |
| | | 520 | | 127 | 80 | 64 |
| | | 530 | | 114 | 69 | 54 |
| | | 540 | | 100 | 60 | 45 |
| | | 550 | | 87 | 51 | 38 |
| | | 560 | | 75 | 44 | 30 |
| | | 570 | | 65 | 37 | 25 |
| | | 580 | | 56 | 32 | 20 |
| X 19 CrMoVNbN 11 1 | 1.4913 | 400 | 0,2 | 262 | 237 | 206 |
| | | 410 | | 257 | 231 | 202 |
| | | 420 | | 252 | 225 | 199 |
| | | 430 | | 246 | 218 | 195 |
| | | 440 | | 240 | 212 | 190 |
| | | 450 | | 234 | 206 | 185 |
| | | 460 | | 228 | 198 | 180 |
| | | 470 | | 221 | 191 | 173 |
| | | 480 | | 214 | 183 | 165 |
| | | 490 | | 207 | 175 | 157 |
| | | 500 | | 199 | 166 | 147 |
| | | 510 | | 190 | 155 | 136 |
| | | 520 | | 181 | 143 | 124 |
| | | 530 | | 171 | 130 | 108 |
| | | 540 | | 160 | 114 | 92 |
| | | 550 | | 149 | 98 | 79 |
| | | 560 | | 134 | 78 | 66 |
| | | 570 | | 118 | 63 | 53 |
| | | 580 | | 100 | 48 | 40 |
| | | 590 | | 80 | 39 | 30 |
| | | 600 | | 61 | 30 | 21 |

¹⁾ The values given in this Table are the mean values of the scatter band so far obtained, which will be checked from time to time as further test results become available and if necessary corrected. A test standard is in preparation.

Table 10. (continued)

| Code number | Material number | Temper-ature °C | for an initial strain ε_A total % | Residual stress in N/mm² after stressing duration for | | | for an initial strain ε_A total % | Residual stress in N/mm² after stressing duration for | | |
|-------------|-----------------|--|---|---|----------|----------|---|---|----------|----------|
| | | | | 1000 h | 10 000 h | 30 000 h | | 1000 h | 10 000 h | 30 000 h |
| NiCr20TiAl | 2.4952 | 450 500 510 520 530 540 550 560 570 580 590 600 610 620 630 640 | 0,15 | 280 | 266 | 256 | 0,20 | 381 | 363 | 342 |
| | | | | 271 | 250 | 234 | | 362 | 335 | 310 |
| | | | | 269 | 245 | 228 | | 356 | 327 | 300 |
| | | | | 266 | 239 | 221 | | 349 | 316 | 288 |
| | | | | 263 | 232 | 213 | | 341 | 305 | 274 |
| | | | | 259 | 225 | 205 | | 331 | 292 | 257 |
| | | | | 255 | 218 | 196 | | 321 | 277 | 237 |
| | | | | 249 | 209 | 187 | | 309 | 260 | 217 |
| | | | | 244 | 201 | 176 | | 296 | 240 | 199 |
| | | | | 238 | 193 | 166 | | 282 | 220 | 182 |
| | | | | 231 | 183 | 155 | | 268 | 200 | 165 |
| | | 650 660 670 680 690 | 0,15 | 224 | 174 | 144 | | 252 | 184 | 149 |
| | | | | 216 | 163 | 133 | | 235 | 169 | 135 |
| | | | | 208 | 153 | 121 | | 221 | 156 | 121 |
| | | | | 200 | 141 | 108 | | 207 | 141 | 108 |
| | | 640 | | 190 | 129 | 96 | | 194 | 130 | 96 |
| | | 700 710 720 730 740 | 0,15 and 0,20 | 181 | 119 | 85 | X | | | |
| | | | | 170 | 107 | 75 | X | | | |
| | | | | 160 | 97 | 65 | X | | | |
| | | | | 149 | 88 | 56 | X | | | |
| | | | | 138 | 79 | 48 | X | | | |
| | | 750 | | 127 | 70 | 40 | X | | | |
| | | | | 117 | 61 | 33 | X | | | |
| | | | | 107 | 53 | 27 | X | | | |
| | | | | 97 | 45 | 22 | X | | | |
| | | | | 88 | 38 | 17 | X | | | |
| | | | | 79 | 31 | 13 | X | | | |

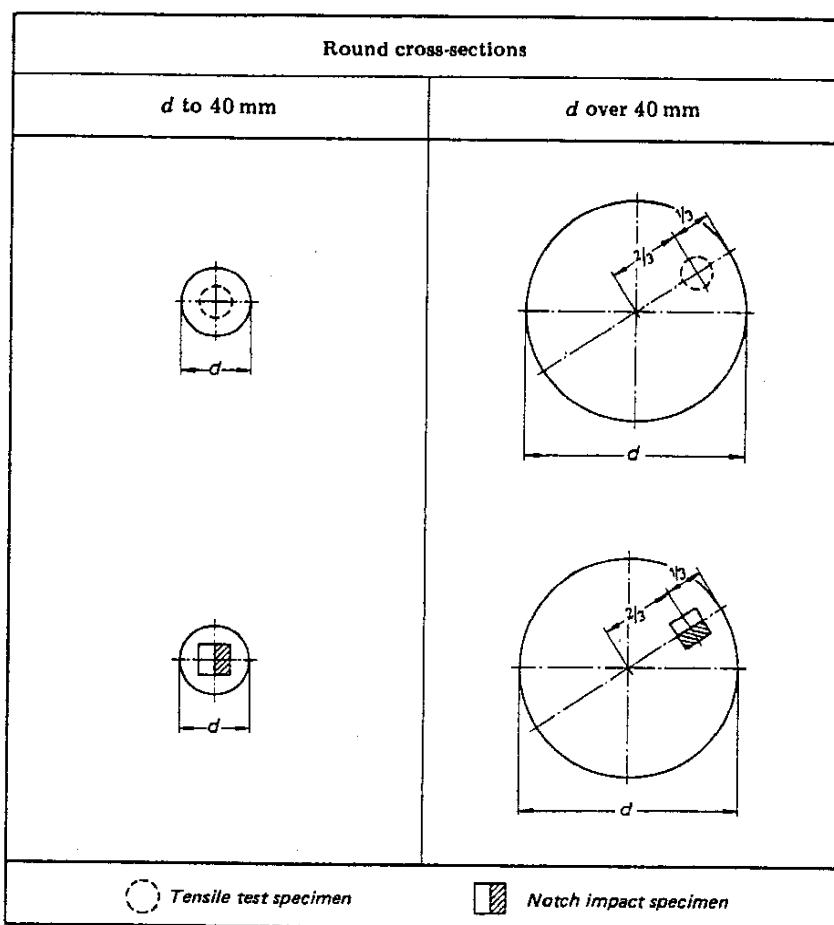


Figure 1. Position of tension and notch impact specimens

The condition "position of specimen axis at $1/6$ along the diameter or diagonal of cross-section of the specimen section or specimen bar" can be complied with for

Tensile test specimens with gripped ends of diameter 10 mm:

- for round steel from about 33 mm diameter
- for square steel from about 39 mm side length.

For notch impact specimens of 10 mm x 10 mm cross-section, the corresponding dimensions shall in each case be about 3 mm larger.

The axis of the notch of the notch impact specimen shall be as far as possible perpendicular to the fibre direction in the material.

The prescribed position from which the specimen is to be taken shall be complied with as precisely as possible.

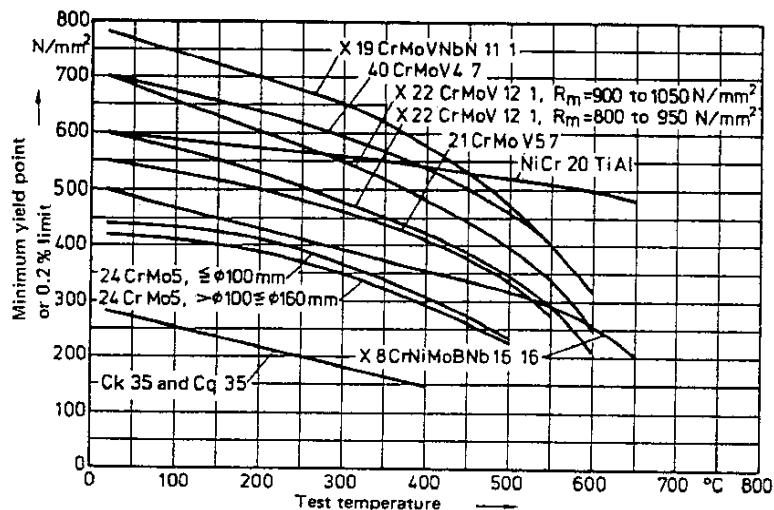


Figure 2. Minimum yield point or 0.2 % limit values as a function of the test temperature (the values in Table 5 apply) (R_m = Tensile strength)

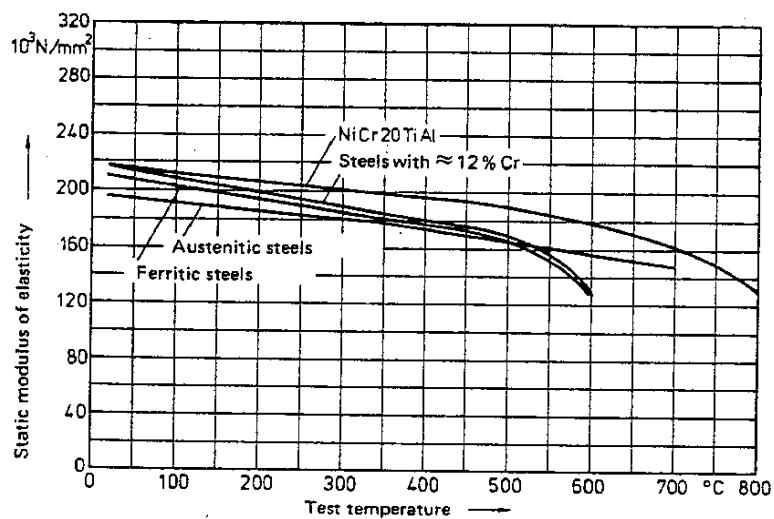


Figure 3. Guide values for the static modulus of elasticity (see also Table 6)

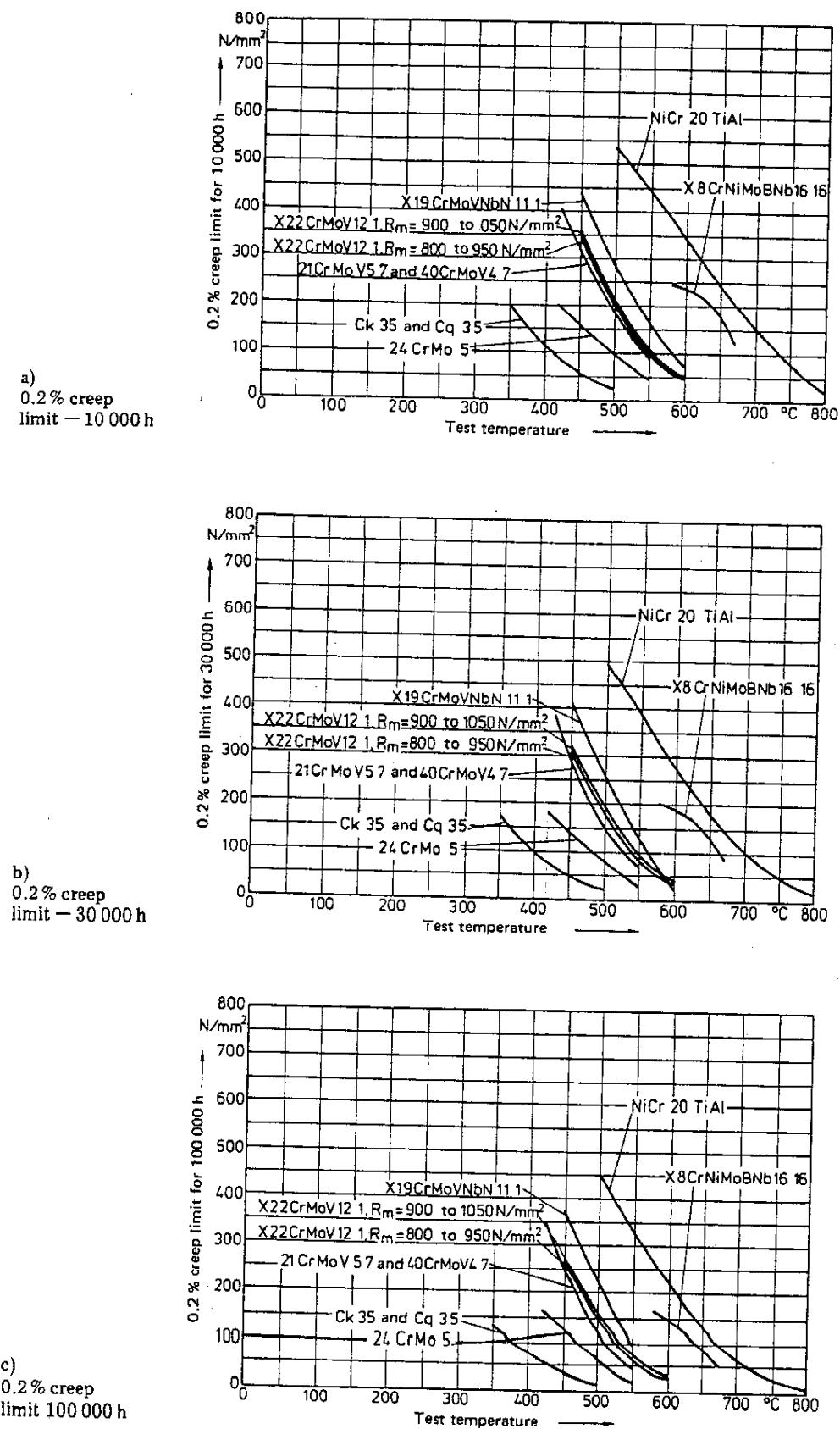


Figure 4. Guide values for the 0.2 % creep limit as a function of temperature (see also Table 9) (R_m = Tensile strength)

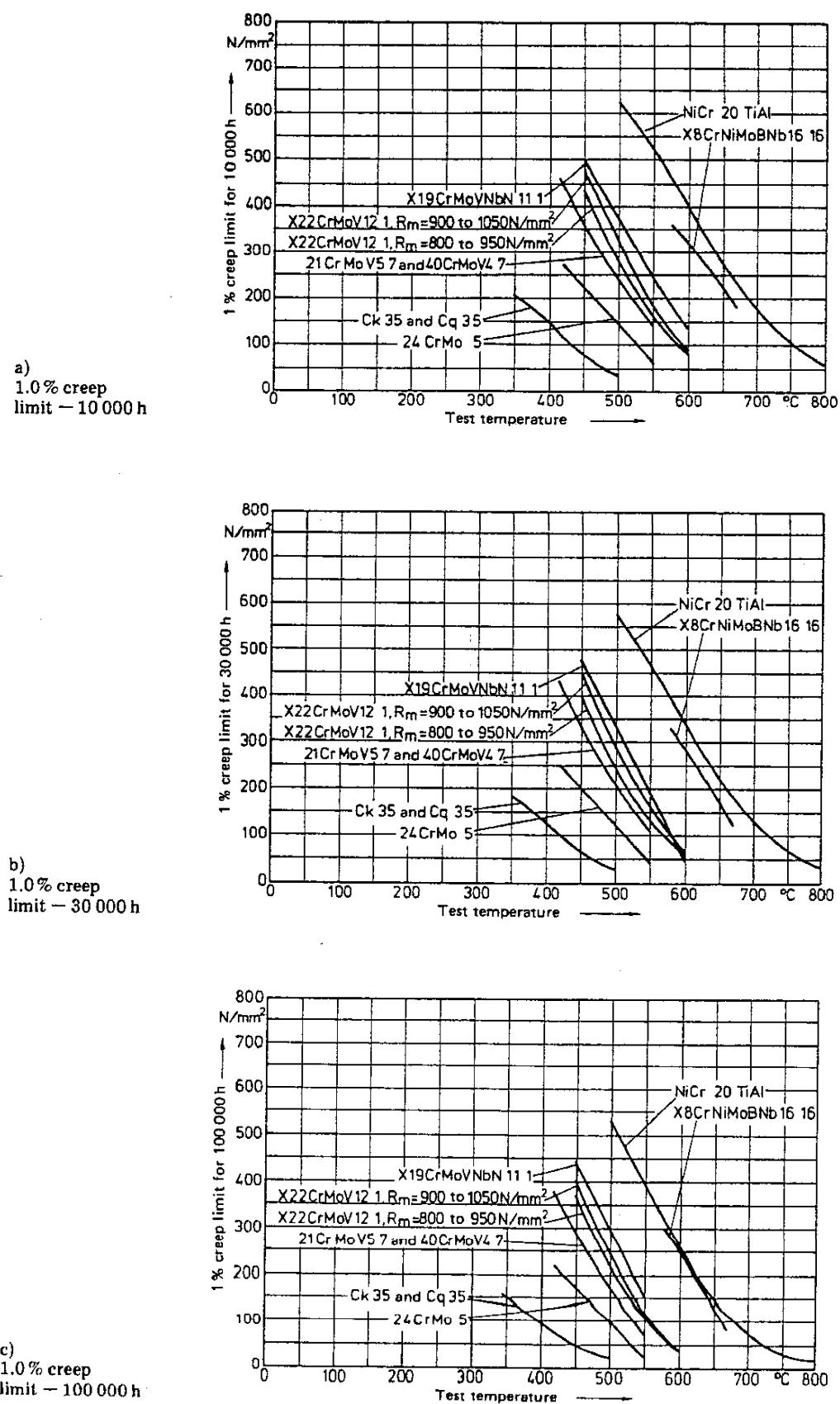


Figure 5. Guide values for the 1.0 % creep limit as a function of temperature (see also Table 9) (R_m — Tensile strength)

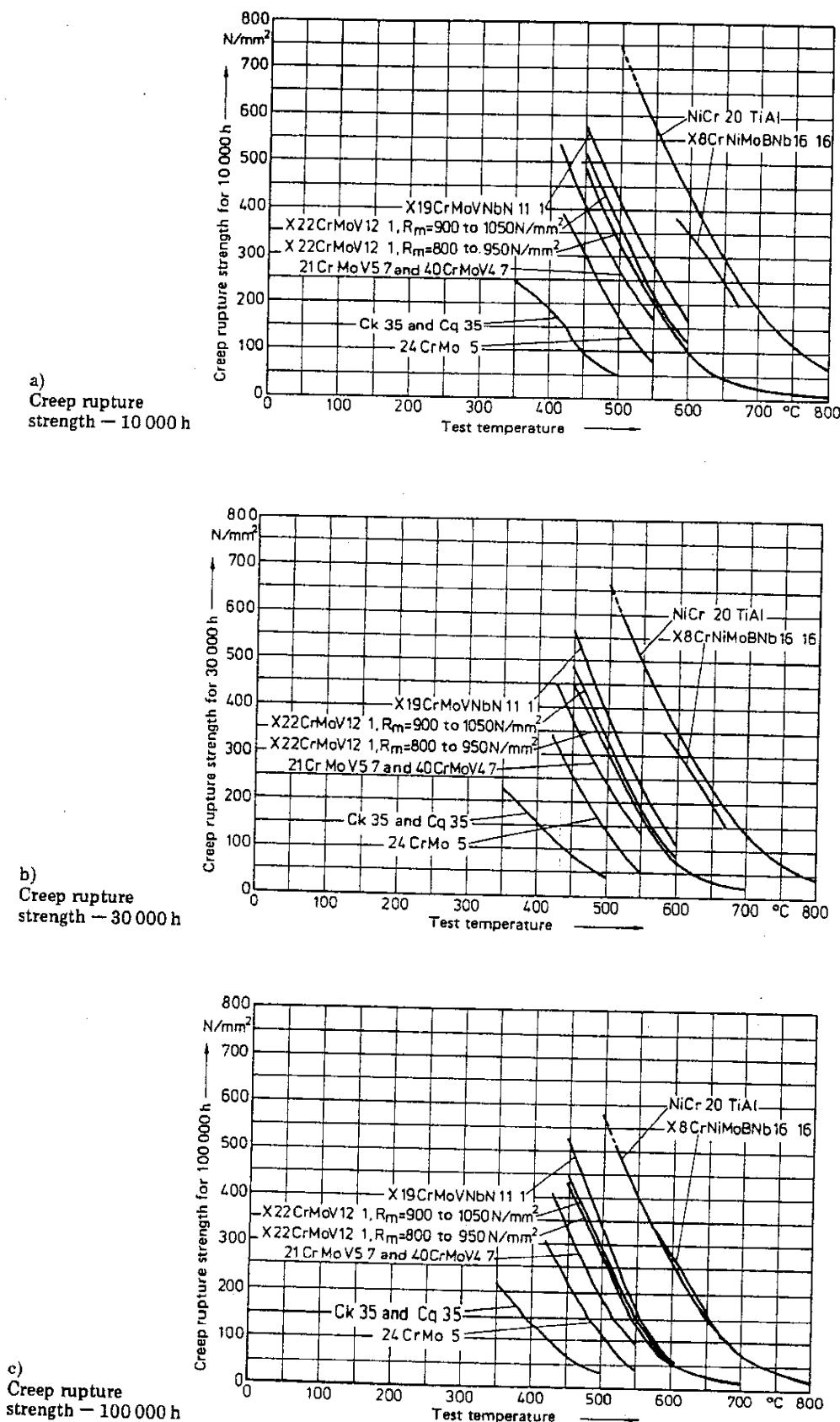


Figure 6. Guide values for the creep rupture strength as a function of temperature (see also Table 9) (R_m = Tensile strength)

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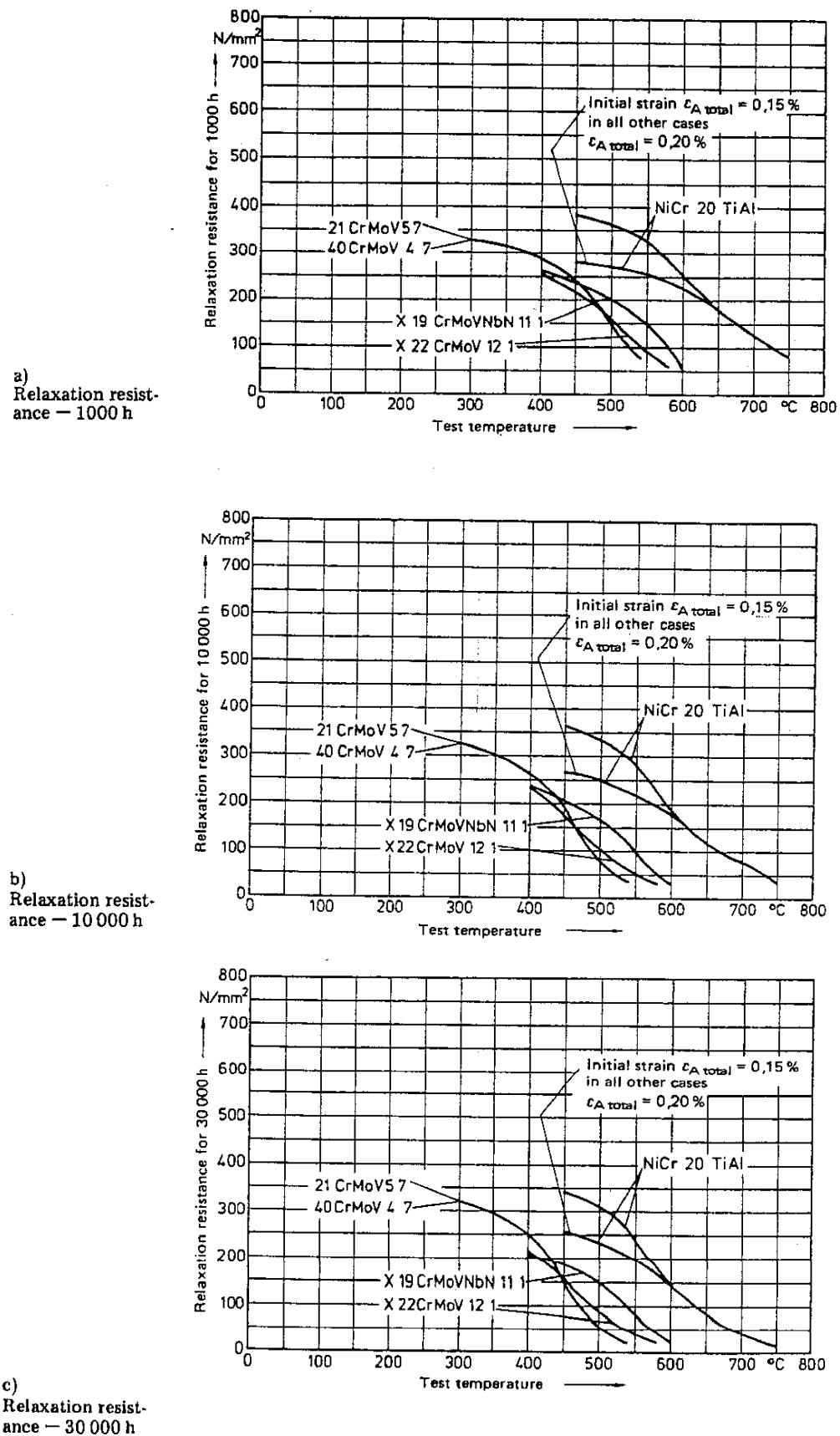


Figure 7. Guide values for the relaxation resistance as a function of temperature (see also Table 10)
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Explanations

This new issue of DIN 17 240 replaces the January 1959 version of Standards DIN 17 240 Part 1 "Heat resisting steels for bolts and nuts; technical conditions of delivery" and Part 2 "Heat resisting steels for bolts and nuts; quality specifications". Its contents differ from the stipulations in the 1959 issues essentially in the following aspects:

1 Selection of materials

The steels

| | |
|----------------|---|
| C 45 | (Material number 1.0503), |
| Ck 45 | (Material number 1.1191), |
| 24 CrMoV 5 5 | (Material number 1.7733), |
| 21 CrMoV 5 11 | (Material number 1.8070) and |
| X 15 CrMo 12 1 | (Material number 1.4920; still material number 1.4921, now obsolete, in the 1959 issue of DIN 17 240) |

have been deleted and the steels or alloys

| | |
|--------------------|------------------------------|
| Cq 35 | (Material number 1.1172), |
| 21 CrMoV 5 7 | (Material number 1.7709), |
| 40 CrMoV 4 7 | (Material number 1.7711), |
| X 19 CrMoVNbN 11 1 | (Material number 1.4913) and |
| NiCr 20 TiAl | (Material number 2.4952) |

have been newly adopted.

The cold upsetting steel Cq 35 is being increasingly used for nuts and smaller diameter screws (to about 20 mm). The grade 21 CrMoV 5 7 replaces the grades 24 CrMoV 5 5 and 21 CrMoV 5 11. On the basis of studies carried out by the Research Association for Heat Resisting Materials, a co-operative body in which steel producers and users are represented, the latter two grades do not, as might be supposed from the guidance values given in DIN 17 240 Part 1 and Part 2, January 1959 issues, have better values than the new grade, particularly with regard to creep behaviour. Bolts and nuts of these two older steels that are still in stock may however be used without reservation in place of bolts or nuts of steel 21 CrMoV 5 7.

The grade 40 CrMoV 4 7 is equivalent to grade B 16 according to ASTM A 193. It is distinguished by the fact that even at 550 °C it still has a relatively high 0.2 % limit values and for this reason and because of the good results obtained with it abroad, has been adopted in DIN 17 240, although it does not fulfil the requirements of the AD Data Sheet (November 1970 issue) (steel bolts and nuts) in respect of DVM absorbed energy ($\geq 8 \text{ kgm/cm}^2$ corresponding to $\geq 55 \text{ J}$ for alloy steels or $\geq 6 \text{ kgm/cm}^2$ corresponding to $\geq 41 \text{ J}$ for unalloyed steels) (see Table 4).

The former nut steel X 15 CrMo 12 1 (material number 1.4920; see above) has been deleted because, on the basis of more recent knowledge on the possibilities of coupling nut and bolt materials, steel X 22 CrMoV 12 1 (material number 1.4923) can be used for both bolts and nuts.

The steel X 19 CrMoVNbN 11 1 (material number 1.4913) and the alloy NiCr20TiAl (material number 2.4952) have been adopted in this Standard because they are being increasingly used.

2 Relaxation resistance

In order to assess the quality of a bolted connection, in general it is important to know the extent to which the materials used tend to lose with time at their service temperature, the initial pre-stress they have been given,

because an increasing proportion of the total strain consists of permanent deformation.

As a supplement to the information on long-time high temperature strength contained in Table 9, Table 10 therefore contains provisional guidance values on the relaxation resistance of the materials in this Standard, expressed in terms of the residual stress as a function of temperature and duration of stressing for a given initial strain on the bolt. These values provide no information on maximum permissible stressing. They do however give an indication as to the intervals at which it is advisable to re-tighten bolted connections in order to restore the required pre-stress. In general, it is advisable to replace bolts after a permanent strain of 1 % has been reached.

The values given in Table 10 are mean values of the scatter band so far recorded. They will be checked from time to time as further test results become available and if necessary corrected. On the basis of information so far available from tests of to $\approx 30\,000$ hours, it can be assumed that the lower limit of this scatter band is about 20 % lower than the quoted mean value at the temperatures given for the steel grades listed.

The values given have been determined in relaxation tests on smooth test bars under uniaxial tensile stress or using the models of bolted connections described in the literature.

3 Absorbed energy

The values of absorbed energy applicable to DVM specimens have in some cases been considerably increased (Table 4) compared with the values formerly stipulated, on the basis of recent statistical evaluations. In addition, minimum values of absorbed energy applicable to ISO V-notch specimens have been adopted in this Standard. In some cases, there was only relatively little test documentation available for these. All those involved are requested to collect and report any further test results on absorbed energy so that the present stipulations can be checked on this basis and if necessary subsequently modified. This applies particularly to the materials newly adopted in the Standard as mentioned above.

4 Transverse specimens

During the discussions, differences of opinion arose as to whether the values given in Tables 4 and 5 for the yield point (or 0.2 % limit) and tensile strength could also be standardized for transverse specimens taken from the core in the case of steel Ck 35 for example. For this reason, as in DIN 17 200 — quenched and tempered steels — sampling has not yet been definitely stipulated in this Standard in the case of transverse specimens, but left open for agreement to be made (see Section 8.3.2).

5 Extent of hardness testing

On the basis of the earlier stipulations (see DIN 17 240 Part 1, Section 3.23, of January 1959 issue) irrespective of the diameter, every bar had to be subjected to a hardness testing in order to check the uniformity of the delivery. On the basis of statistical evaluations on uniformity of deliveries and the use of special processes for monitoring uniformity of the products in a number of manufacturing works, it has been possible to eliminate this testing effort completely (see Section 8.2.3). According to the circumstances of individual manufacturers, agreements should be made for a further reduction in the extent of testing.